OSCILLATOR STRENGTHS FOR DIPOLE-ALLOWED FINE-STRUCTURE TRANSITIONS IN SI II

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An extensive dataset of oscillator strengths, line strengths, and Einstein A-coefficients has been calculated for a large number of dipole-allowed ($\Delta S=0$) fine-structure transitions in Si II. The line strengths in LS coupling are obtained in an ab initio manner in the close-coupling approximation employing the R-matrix method. The fine-structure components are obtained through algebraic transformations of the LS multiplets. Observed spectroscopic energies are employed whenever available. A 12-state eigenfunction expansion of the core ion, Si III, is employed for the present calculations. This work presents the oscillator strengths of 1122 fine-structure transitions in Si II corresponding to 390 LS multiplets and provides a reasonably complete set of radiative transitions for this astrophysically important ion for the first time. Present results are of comparable accuracy to previous detailed calculations obtained for a small number of transitions and are in reasonably good agreement with the measured oscillator strengths and lifetimes. © 1998 Academic Press

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INTRODUCTION

Si II is one of the most common ions observed in absorption and emission spectra from astrophysical sources, such as the interstellar medium, quasars, hot stars, and the sun. The oscillator strengths for transitions in Si II are used in the determination of abundances, temperatures, densities, and column densities (see, e.g., Ref. [1]). Si II has been investigated both experimentally [2–9] and theoretically [10–17] by many workers. However, all these studies have remained confined to a limited number of transitions until the work of the Opacity Project (OP) [10]. One of the aims of the OP [18] has been to obtain accurate atomic radiative data in an ab initio manner in the close-coupling (CC) approximation using the R-matrix method. The radiative work of the OP was carried out in LS coupling; however, the laboratory plasma experiments and the various astrophysical models usually consider the fine-structure transitions (see, e.g., [2-5]). The extended non-LTE (low temperature equilibrium) models which consider a number of transitions, such as ones observed in hot stars, require both radiative and collisional data for a large number of energy levels. Collisional data are now available for Si II [19] obtained in the close-coupling approximation using the R-matrix method. The aim of this work is to present an extensive set of radiative data of reliable accuracy for fine-structure transitions in Si II to be used in collisional-radiative models employed in astrophysical applications. Similar sets of data for fine-structure transitions in other ions employing the present method have been reported earlier [20].

Summary of the Theoretical Work and Computations

The calculations of the oscillator strengths (*f*-values), line strengths (*S*-values), and Einstein coefficients

or transition probabilities (*A*-values) have been described in previous works [20] and are not discussed in detail here. We present only the computational details pertaining to the Si II calculations.

In terms of accuracy, the strength of the present method lies in the fact that accurate bound-state wavefunctions may be obtained for an atom or ion using the close-coupling approximation where the core ion, termed the "target," represents the N-electron system. The wavefunction expansion, $\Psi(E)$, for any symmetry, $SL\pi$, of the bound (N+1) electron system is represented in terms of the target states as

$$\Psi(E) = \mathbf{A} \sum_{i} \chi_{i} \theta_{i} + \sum_{j} c_{j} \Phi_{j}, \tag{1}$$

where χ_i is the target ion wavefunction in a specific state $S_i L_i \pi_i$ and θ_i is the wave function for the (N+1)th electron in a channel labeled as $S_i L_i \pi_i k_i^2 l_i (SL\pi)$; k_i^2 is the electron energy, which for $k_i^2 < 0$ may represent bound states of the e+i on system; and \mathbf{A} is the antisymmetrization operator. The Φ_j 's are correlation functions of the (N+1) electron system that compensate for the orthogonality condition on the total wavefunction, as well as account for short-range correlation effects, and c_j 's are the variational coefficients. The CC expansions imply extensive configuration interactions in the coupled wave functions for each $SL\pi$ at negative energies corresponding to the bound states of the system.

The present work corresponds to CC calculations employing a 12-state expansion of the target ion Si III. The target states are: $3s^2(^1S^e)$, $3s3p(^3P^o, ^1P^o)$, $3p^2(^1D^e, ^3P^e, ^1S^e)$, $3s3d(^3D^e, ^1D^e)$, $3s4s(^3S^e, ^1S^e)$, $3s4p(^3P^o, ^1P^o)$. These states are optimized through atomic structure calculations with spectroscopic con-

figurations, $3s^2$, 3s3p, $3p^2$, 3s3d, 3s4s, 3s4p, and correlation configurations, $3d^2$, 3p3d, 3p4s, 3p4p, 3d4s, 3d4p.

Computations for the line strengths are carried out employing the R-matrix codes developed for the OP [21]. We obtain 65 calculated bound *LS* states of Si II below the first ionization threshold and 390 corresponding oscillator strengths for transitions among these states. The number of observed energy terms [22] is 45. The calculated energies agree within 3% with the measured ones for most of the states, as can be seen in Table I.

The fine-structure components of the transitions are obtained through algebraic transformations of the LS multiplet in the two ways as described in Ref. [20] and employing the code JJTOLS [20]. The f, S, and A are related as

$$E_{fi} = 3g_i(f_{if}/S), \quad A_{fi}(\text{a.u.}) = \frac{1}{2}\alpha^3 \frac{g_i}{g_f} E_{fi}^2 f_{if},$$

$$A_{fi}(\text{s}^{-1}) = \frac{A_{fi}(\text{a.u.})}{\tau_0}, \quad (2)$$

where E_{fi} is the transition energy in rydbergs; S is the line strength in atomic units (a.u.), α is the fine structure constant; g_i , g_f are the statistical weight factors of the initial and final states [g = (2S + 1)(2L + 1)] in LS coupling and = (2J + 1) in JJ coupling]; and τ_0 = 2.4191×10^{-17} s is the atomic unit of time. Spectroscopic observed energies [22] are employed whenever available as these are measured with higher accuracy than the calculated values. As the present calculated energies agree quite well with the observed energies for most of the terms, implementation of the observed energies improves the accuracies of the total f- and A-values only slightly. Table I lists all the bound LS terms among which the dipole allowed fine-structure transitions are considered, resulting in 1122 transitions. In Table I, each LS term is prefixed by a degeneracy symbol for convenience of identification, in accordance with the National Institute of Standards and Technology convention. An alphabetically ascending order of letters is chosen for the even parity states and a descending order for the odd parity states of the same symmetry.

The target expansion in this work is the same as that which Mendoza et al. [10] used for the OP radiative data. The R-matrix computations are carried out independently in both works. Although the level of accuracy in both the works is about the same, the extent of the present computations is not exactly the same as that of theirs. (The details of the OP work are yet to be published.) The differences between the two works come from the choice of number of terms in the R-matrix basis set, number of partial waves, and number of bound channels in the second sum of the CC expansion [Eq. (1)], all of which

affect the accuracy of the calculations. The R-matrix basis set of 12 terms in the present work was checked for convergence through unitarity of collision strengths for excitation and dielectronic recombination as in Ref. [23]. All possible configurations of the ion were included in the bound channel second term of the CC expansion to complete the electron correlation effects. A larger number of partial waves is included, *l* going up to 9 in the present work as compared to 5 in the OP work, and this has resulted in a larger data set.

Results and Discussion

The f-, S-, and A-values for the 1122 dipole-allowed fine-structure transitions in Si II, corresponding to 390 LS multiplets, have been calculated. The complete set of f-values is presented in Table II; a computer-readable listing including S- and A-values is available electronically from the author at the address given at the end of the Conclusion.

To evaluate the uncertainties, comparison of the present weighted oscillator strengths gf is made for astrophysically important transitions with a number of other available theoretical and experimental values in Table A. Although the multiplet transitions have been studied more extensively for a number of transitions, much less data are available for the fine-structure transitions. Among the calculations, Mendoza et al. [10] and the present work correspond to ab initio R-matrix calculations which can be used for large-scale computations of the f-values. Most other works correspond to various atomic structure calculations requiring optimization and can be applied for a limited number of transitions. Differences in optimization may lead to differences in results as we discuss below, where comparison of the present results is made with some of the best results available at this time.

For the transition $3s^23p(z^2P^o) \rightarrow 3s3p^2(a^2P^e)$, the only other calculated gf-values available for the finestructure components are by Luo et al. [15]. As can be seen in Table A, the present gf-values show good agreement with those of Luo et al. [15], while the measured values are about 17% lower. For the multiplet transition the present gf-value agrees consistently well with all other calculated numbers, but the measured values are again somewhat lower than the calculated values. The transition $3s^23p(z^2P^o) \rightarrow 3s3p^2(a^2D^e)$ has been studied by a number of investigators, but both the measured and the calculated values show a large spread. This is a rather sensitive transition because the upper a^2D^e state is a mixture of $3s3p^2$ and $3s^23d$ which causes cancellations in the relevant matrix elements. The latest measurement for both the LS and the fine-structure transitions of $3s^23p(z^2P^o) \rightarrow 3s3p^2(a^2D^e)$ was carried out by Berjeson and Lawler [2]. The agreement of their

TABLE A
Comparison of the Present gf-values with Experiments and Other Calculations

		LS multiplet	t			Fine structure				
Transition	Present	Expt	Theo	g_i	g_f	Present	Expt	Theo		
$3s^23p(z^2P^o) \rightarrow 3s3p^2(a^2P^e)$	5.233	4.5 [5]	5.226 [13]	4	4	2.906		2.943 [15]		
		4.32 [4]	5.32 [14]	4	2	0.580		0.607 [15]		
		4.44 [7]	5.28 [15]	2	4	0.583	0.489 [4]	0.587 [15]		
			5.32 [10] 5.46 [17]	2	2	1.164	0.964 [4]	1.159 [15]		
$3s^23p(z\ ^2P^o) \rightarrow 3s3p^2\ (a\ ^2D^e)$	0.0148	0.0112 [2] 0.0312 [4] 0.033 [5]	0.0149 [10] 0.0099 [11] 0.0112 [13] 0.0208 [15]	2	4	0.0049	0.00417 [2] 0.0103 [4] 0.0110 [5] 0.00631 [8]	0.00631 [12] 0.00626 [15]		
			0.0060 [16]	4	6	0.00880	0.00661 [2] 0.0198 [5]	0.00646 [12] 0.0108 [15]		
				4	4	0.00098	0.000513 [2] 0.00220 [5]	0.000398 [12] 0.00116 [15]		
$3s^23p(z^2P^o) \to 3s^23d(b^2D^e)$	7.104	6.84 [7]	7.07 [10]	4	4	0.473		0.46 [15]		
1 (-)		5.76 [5]	6.98 [13]	4	6	4.26		4.18 [15]		
		5.1 [4]	7.17 [11] 6.97 [15] 6.83 [16]	2	4	2.374	1.70 [4]	2.32 [15]		
$3s^23p(z^2P^o) \to 3s^24d(c^2D^e)$	0.971	0.96 [4]	1.02 [10]	4	4	0.065	0.053 [5]			
	0.571	0.798 [5]	1.44 [11]	4	6	0.582	0.477 [5]			
		[6]	1.05 [13] 1.62 [15]	2	4	0.324	0.320 [4] 0.266 [5]	0.403 [15]		
			1.10 [16]							
$3s^23p(z^2P^o) \to 3s^24s(a^2S^e)$	0.802	1.38 [5]	0.786 [10]	4	2	0.534	0.916 [5]	0.467 [15]		
	*****	1.23 [4]	0.773 [11]	2	2	0.268	0.460 [5]	0.233 [15]		
		[-]	0.780 [13] 0.78 [17]				0.414 [4]			
$3s^23p(z^2P^o) \to 3s3p^2(b^2S^e)$	0.504	0.882 [5]	0.531 [10]	4	2	0.336	0.587 [5]	0.353 [15]		
1 . ,		0.822 [4]	0.633 [11]	2	2	0.168	0.294 [5]	0.203 [15]		
			0.529 [13] 0.548 [15] 0.54 [17]				0.272 [4]			
$3s^23p(^2P^o) \to 3s^25s(c^2S^e)$	0.087	0.169 [5]	0.090 [10]	4	2	0.058	0.113 [5]			
55 5p(1) 55 55(C 5)	0.007	0.107 [3]	0.119 [13]	2	2	0.038	0.56 [5]			

measured LS multiplet value with the present f-value is fair, while the agreement is good with the present J=1/2-3/2 fine-structure component. Their results also agree well with the atomic structure calculations of Hibbert et al. [13] for the LS multiplet and reasonably well with those of Dufton et al. [12] for the fine-structure transitions. The present gf value agrees quite well with that given by Mendoza et al. [10] for this transition and for other transitions. For the second transition of this symmetry, $z^2P^o \rightarrow b^2D^e$, good agreement is found between the present value with the measured value of Livingston et al. [7] and with all other theoretical calcu-

lations. The fine-structure components agree well with Luo et al. [15], while the measured value [4] is lower. For the third transition, $z^2P^o \rightarrow c^2D^e$, the present gf value agrees very well with the measured value of Van Buren [4] and with a few of the other theoretical values [10, 13, 16]. For the three transitions $z^2P^o \rightarrow (a, b, c)^2S^e$, all the calculated values agree with each other in general, but the measured values show poor agreement with the calculations.

Comparison is also made of the present lifetimes with other measured and calculated values in Table B. The lifetimes can be measured in general with less uncer-

TABLE B

Comparison of the Present Lifetimes (τ) with Experiments and Other Calculations

		τ (ns)	
State	Present	Experiment	Theory
$z^{4}S^{o}$	0.270	0.35 (.1) [8]	0.258 [10] 0.27 [14]
a^2D^e	335.7	439 (44) [2] 200–400 [9]	342 [10] 442 [13] 210.5 [14] 850 [16] 128 [17]
$b^{2}D^{e}$	0.337	0.35 (.04) [7] 0.7 (.2) [9] 0.45 (.05) [8]	0.339 [10] 0.343 [13] 0.35 [16] 0.37 [14]
a^2P^e	0.245	0.29 (.04) [7] <0.4 [9]	0.33 [17] 0.235 [10] 0.246 [13] 0.23 [14]
a^2S^e	0.876	0.89 (.05) [3] 0.91 (.04) [3] 0.9 (.2) [9]	0.26 [17] 0.901 [10] 0.904 [13] 0.83 [14]
b^2S^e	1.017	0.58 [5]	0.90 [17] 0.929 [10] 0.968 [13] 1.08 [14] 0.94 [17]
$c^{-2}S^e$	2.552	1.99 (.2) [3]	2.36 [10] 2.501 [13]
y ² P °	9.478	8.3 (.8) [8] 9.1 (5) [6]	9.31 [10] 9.51 [13] 9.7 [16] 8.29 [14]
z^2F^o	3.355	3.2 (.4) [9] 3.4 (3) [6]	3.26 [10] 3.1 [16]

Note. Numbers in parentheses give the experimental errors.

tainty than the gf values. The lifetime value is obtained easily once the A-values are known since

$$\tau_f = \frac{1}{A_f} \,, \tag{3}$$

where A_f is the total radiative transition probability for the state f, i.e.,

$$A_f = \sum_i A_{fi}. \tag{4}$$

The present lifetime of the state z^4S^o agrees with the calculations by Mendoza et al. [10] and Hjorth-Jensen and Aashmar [14], but is lower than the measured value by Berry et al. [8]. The lifetime of the a^2D^e state of the present work is within the spread of various measured

values and agrees closely only with the value calculated by Mendoza et al. [10]. However, the measured lifetime of the a^2D^e state by Berjeson and Lawler [2] agrees very well with the atomic structure calculations of Hibbert et al. [13], which is expected since both groups agree well with each other for the relevant gf values. As in the case of the gf value, the present lifetime for the b^2D^e state agrees well with the value measured by Livingston et al. [7] and with all calculated values. The present lifetime for $a^{2}P^{e}$ is consistent with all other calculated values and with the measured values of Livingston et al. [7] and of Savage and Lawrence [9]. Good agreement is obtained among the calculated and measured lifetimes for a^2S^e . The measured lifetime of b^2S^e is much lower than all the calculated values. The present lifetime for the $c^{-2}S^e$ state is about 28% larger than the recent value measured by Schectman and Povolny [3], but agrees very well with the value calculated by Hibbert et al. [13]. Good agreement is achieved among calculated and measured lifetime values for the states y^2P^o and z^2F^o .

An estimate of the accuracy for the present f-, S-, and A-values is approximately 10–30% for most of the transitions, based on the general uncertainty estimate in the close-coupling method, the low uncertainty in the calculated energy values, and the comparison of the gf and lifetime values with those given in other works. For weak transitions, the uncertainties can be larger. A few points should be noted as follows. The present method obtains the fine-structure components through a purely algebraic transformation and does not include any relativistic mixing of LS terms explicitly in the wave functions. Hence, for the transitions between highly excited states, the uncertainty may be higher if LSJ-mixing becomes significant. Intercombination transitions between levels of different spin multiplicity could then redistribute the line strengths somewhat differently among the allowed finestructure components.

Conclusion

A reasonably complete set of f-, S-, and A-values for 1122 dipole-allowed fine-structure transitions in Si II is obtained for the first time. The values should be accurate to within 10–30%. The uncertainty due to neglect of relativistic effects is expected to be low for this singly charged ion. However, the uncertainty for transitions among highly excited levels may be higher owing to intermediate-coupling effects. Present results should be applicable to detailed analysis of the absorption and emission spectra of Si II from a variety of astrophysical sources.

The full table of transition probabilities and energies is available in electronic form from the author at nahar @astronomy.ohio-state.edu. A FORTRAN77 code is also attached to the table to read the *A*-values and calculate the lifetimes for any *LS* term or fine-structure level.

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EXPLANATION OF TABLES

TABLE I. Bound States of Si II

This table presents the bound states of Si II among which the dipole allowed transitions are considered.

- Term Electronic configuration and *LS* term. Each *LS* term is prefixed by a degeneracy symbol in alphabetically ascending order for successive even parity and descending order for successive odd parity states of the same symmetry
- $E_{expt}(Ry)$ Experimental term binding energies of Si II (in rydbergs), derived from statistically averaging over the measured levels of Si II from Ref. [22]
- $E_{cal}(Ry)$ Term binding energies (in rydbergs) obtained in the present calculations

TABLE II. Energies and Oscillator Strengths for Allowed Transitions in Si II

In Table II, data are given in subsets, with the first line corresponding to the LS transition and subsequent lines to its fine-structure components. The subsets are ordered by observed states up to $a^4P^e \rightarrow z^4D^o$ followed by the calculated states starting with transition $h^2S^e \rightarrow q^2P^o$. The calculated transition energy is used for a transition where one or both states are unobserved.

Transition The transition $i \to f$, with states i and f in the notation of Table I

- E_i , E_f Term binding energies of the initial and final LS terms given in rydberg on the first line and the excitation energies of the initial and final fine structure levels given in cm⁻¹ in subsequent lines. Negative signs for LS term binding energies are omitted for convenience. For transitions between observed levels, experimental energies are listed. For transitions where one or both states are unobserved, theoretical binding energies are listed and no calculated fine-structure energies are given. The energy for these latter transitions can be obtained as $E_{fi} = 3g_i(f_{if}/S)$ from the f- and S-values given in the electronic version of the table.
- g_i , g_f The statistical weight factors of the initial and final states f_{if} Oscillator strength

TABLE I. Bound States of Si II See page 189 for Explanation of Tables

Term		$E_{expt}(Ry)$	$E_{cal}(Ry)$	Term	1	$E_{expt}(Ry)$	$E_{cal}(Ry)$
$-3s^{2}4s$	a^2S^e	-0.604586	-0.6019	$3s^26f$	x^2F^o	-0.114226	-0.1141
$3s3p^{2}$	$b^{-2}S^e$	-0.502844	-0.4892	$3s^27f$	$w^{\ 2}F^o$	-0.083752	-0.0836
$3s^{2}5s$	$c^{-2}S^e$	-0.308682	-0.3072	$3s^{2}8f$	v^2F^o	-0.064007	-0.0639
$3s^26s$	$d^{\ 2}S^e$	-0.188283	-0.1870	$3s^{2}9f$	$u^{2}F^{o}$	-0.050496	-0.0504
$3s^{2}7s$	$e^{\ 2}S^e$	-0.126951	-0.1262	$3s^210f$	$t^{-2}F^o$	-0.040848	-0.0408
$3s^{2}8s$	$f^{-2}S^e$	-0.091416	-0.0909	$3s^{2}5g$	$a^{\ 2}G^e$	-0.161012	-0.1608
$3s^{2}9s$	extstyle e	-0.068977	-0.0687	$3s^26g$	$b^{\ 2}G^e$	-0.111793	-0.1117
$3s^{2}10s$	$h^{-2}S^e$		-0.0537	$3s^27g$	$c^{\ 2}G^e$	-0.082114	-0.0820
$3s^{2}11s$	$i\ ^2S^e$		-0.0431	$3s^{2}8g$	$d^{\ 2}G^e$	-0.062856	-0.0628
$3s3p^2$	$a^{\ 2}P^e$	-0.436581	-0.4270	$3s^{2}9g$	$e^{\ 2}G^e$	-0.049660	-0.0496
$3s3p(^{3}P^{o})4p$	$b\ ^2P^e$		-0.0064	$3s^{2}10g$	$f^{\ 2}G^e$	-0.040224	-0.0402
$3s^23p$	$z\ ^2P^o$	-1.199725	-1.2014	$3s^{2}6h$	$z^{-2}H^o$		-0.1112
$3s^24p$	$y^{2}P^{o}$	-0.461236	-0.4637	$3s^27h$	y^2H^o		-0.0817
$3s^25p$	x^2P^o	-0.254872	-0.2564	$3s^{2}8h$	x^2H^o		-0.0626
$3s^26p$	w^2P^o	-0.162882	-0.1625	$3s^29h$	w^2H^o		-0.0494
$3s^{2}7p_{\perp}$	v^2P^o	-0.114654	-0.1165	$3s^{2}10h$	v^2H^o		-0.0400
$3s3p(^{3}P^{o})4s$	u^2P^o	-0.093902	-0.1011	$3s^27i$	$a^{2}I^{e}$		-0.0816
$3s^28p$	$t^{2}P^{o}$	-0.079472	-0.0802	$3s^{2}8i$	$b^{2}I^{e}$		-0.0625
$3s^29p$	s^2P^o	-0.062106	-0.0622	$3s^29i$	$c^{\ 2}I^e$		-0.0494
$3s3p(^3P^o)3d$	r^2P^o	-0.050990	-0.0525	$3s^{2}10i$	$d^{2}I^{e}$		-0.0400
$3s^210p$	$q^{2}P^{o}$	-0.048422	-0.0481	$3s_{2}^{2}8k$	$z^{2}K^{o}$		-0.0625
$3s3p^2$	$a^{2}D^{e}$	-0.697367	-0.7091	$3s^{2}9k$	y^2K^o		-0.0494
$3s_{2}^{2}3d$	b^2D^e	-0.478394	-0.4787	$3s^{2}10k$	$x^{2}K^{o}$		-0.0400
$3s^24d$	c^2D^e	-0.280873	-0.2796	$3s^{2}9l$	a^2L^e		-0.0494
$3s^{2}5d$	d^2D^e	-0.177254	-0.1763	$3s^{2}10l$	$b^{2}L^{e}$		-0.0400
$3s^{2}6d$	$e^{2}D^{e}$	-0.121410	-0.1209	$3s^{2}10m$	$z^{2}M^{o}$		-0.0400
$3s^27d$	f^2D^e	-0.088234	-0.0879	$3p^3$	z $^4S^o$	-0.080306	-0.0868
$3s_{2}^{2}8d$	g^2D^e	-0.066982	-0.0668	$3s3p^2$	a^4P^e	-0.809605	-0.8284
$3s_{2}^{2}9d$	h^2D^e		-0.0524	$3s3p(^3P^o)4s$	z^4P^o	-0.134751	-0.1497
$3s^210d$	$i^{2}D^{e}$		-0.0422	$3s3p(^3P^o)3d$	y^4P^o	-0.066073	-0.0769
$3s3p(^{3}P^{o})3d$	z^2D^o	-0.209976	-0.2302	$3s3p(^{3}P^{o})3d$	z^4D^o	-0.068094	-0.0801
$3s^{2}4f$	$z^{2}F^{o}$	-0.257797	-0.2477	$3s3p(^3P^o)3d$	$z\ ^4F^o$	-0.158839	-0.1765
$3s^25f$	y^2F^o	-0.164810	-0.1646				

TABLE II. Energies and Oscillator Strengths for Allowed Transitions in Si II See page 189 for Explanation of Tables

Transition	$\frac{E_i}{\mathrm{Ry/cm^{-1}}}$	$\frac{E_f}{\mathrm{Ry/cm^{-1}}}$	g_i	g_f	f_{if}	Transition	E_i	E_f	g_i	g_f	f_{if}
	ку/сш	ny/cm					Ry/cm ⁻¹	Ry/cm ⁻¹			
$a^2S^e o y^2P^o$	0.6046	0.4612	2 2	6	1.136E+00	$c^2S^e \rightarrow q^2P^o$	0.3087	0.0484	2	6	7.885E-04
	65500.47	81251.32	2	4	7.582E-01	•	97972.09	126525.80	2	4	5.256E-04
$a^2S^e \rightarrow x^2P^o$	65500.47	81191.34	2	2 6	3.776E-01	22.00	97972.09	126545.40	2	2	2.630E-04
$a^-S^- \rightarrow x^-F^-$	$0.6046 \\ 65500.47$	$0.2549 \\ 103885.25$	$\frac{2}{2}$	4	4.059E-03 2.707E-03	$d^2S^e \to w^2P^o$	0.1883 111184.46	$0.1629 \\ 113976.72$	$\frac{2}{2}$	6 4	2.027E+00 1.354E+00
	65500.47	103860.74	$\tilde{2}$	$ar{2}$	1.352E-03		111184.46	113962.08	$\frac{2}{2}$	2	6.733E-01
$a^2S^e \rightarrow w^2P^o$	0.6046	0.1629	2	6	8.796E-03	$d^2S^e \rightarrow v^2P^o$	0.1883	0.1147	2	6	3.164E-02
	65500.47 65500.47	113976.72	$\frac{2}{2}$	4 2	5.865E-03 2.931E-03		111184.46	119273.81	2	4	2.112E-02
$a^2S^e \rightarrow v^2P^o$	0.6046	$\begin{array}{c} 113962.08 \\ 0.1147 \end{array}$	2	6	2.089E-02	$d^2S^e \rightarrow u^2P^o$	111184.46 0.1883	119245.22 0.0939	2	2 6	1.052E-02 9.998E-02
u b =/ 0 1	65500.47	119273.81	2 2	4	1.393E-02	$u^-S^- \rightarrow u^-F^-$	111184.46	121590.19	$\frac{2}{2}$	4	6.697E-02
0 0	65500.47	119245.22		2	6.962E-03		111184.46	121444.12	2	2	3.301E-02
$a^2S^e o u^2P^o$	$0.6046 \\ 65500.47$	0.0939 121590.19	$\frac{2}{2}$	6 4	1.239E-02 8.267E-03	$d^2S^e o t^2P^o$	0.1883	0.0795	2	6	5.807E-03
	65500.47	121444.12	$\frac{2}{2}$	2	4.123E-03		111184.46 111184.46	123138.67 123097.63	2 2	4 2	3.876E-03 1.931E-03
$a^2S^e \rightarrow t^2P^o$	0.6046	0.0795	2	6	8.304E-05	$d^2S^e \rightarrow s^2P^o$	0.1883	0.0621	$\tilde{2}$	6	6.167E-05
	65500.47	123138.67	2	4	5.537E-05		111184.46	125033.70	2	4	4.112E-05
.2 ce2 Do	65500.47	123097.63	2	2	2.767E-05	12 ce 2 Do	111184.46	125024.90	2	2	2.055E-05
$a^2S^e \rightarrow s^2P^o$	$0.6046 \\ 65500.47$	$0.0621 \\ 125033.70$	$\frac{2}{2}$	6 4	1.086E-03 7.237E-04	$d^2S^e \rightarrow r^2P^o$	0.1883 111184.46	$0.0510 \\ 126236.40$	$\frac{2}{2}$	6 4	7.656E-03 5.099E-03
	65500.47	125024.90	$\tilde{2}$	$\overline{2}$	3.618E-04		111184.46	126279.00	$\tilde{2}$	$\overline{2}$	2.557E-03
$a^2S^e \rightarrow r^2P^o$	0.6046	0.0510	2	6	3.330E-03	$d^2S^e \rightarrow q^2P^o$	0.1883	0.0484	2	6	2.910E-03
	65500.47	126236.40	$\frac{2}{2}$	$\frac{4}{2}$	2.220E-03 1.111E-03		111184.46	126525.80	2	4	1.939E-03
$a^2S^e \rightarrow q^2P^o$	65500.47 0.6046	126279.00 0.0484	2	6	8.135E-06	$e^2S^e \rightarrow v^2P^o$	$\begin{array}{c} 111184.46 \\ 0.1270 \end{array}$	$126545.40 \\ 0.1147$	2	2 6	9.708E-04 1.610E+00
u D / 4 1	65500.47	126525.80	2	4	5.422E-06	e 5 - 7 v 1	117914.80	119273.81	$\frac{2}{2}$	4	1.081E+00
.0	65500.47	126545.40	2	2	2.712E-06		117914.80	119245.22	2	2	5.291E-01
$b^2S^e \rightarrow y^2P^o$	0.5028	0.4612	$\frac{2}{2}$	6 4	5.262E-03	$e^2S^e o u^2P^o$	0.1270	0.0939	2	6	1.396E+00
	76665.35 76665.35	$81251.32 \\ 81191.34$	$\frac{2}{2}$	2	3.524E-03 1.739E-03		117914.80 117914.80	$\begin{array}{c} 121590.19 \\ 121444.12 \end{array}$	$\frac{2}{2}$	$\frac{4}{2}$	9.430E-01 4.527E-01
$b^2S^e \rightarrow x^2P^o$	0.5028	0.2549	2	6	3.899E-04	$e^2S^e \rightarrow t^2P^o$	0.1270	0.0795	2	6	5.068E-02
	76665.35	103885.25	2	4	2.600E-04		117914.80	123138.67	2	4	3.387E-02
$b^2S^e \rightarrow w^2P^o$	76665.35 0.5028	$103860.74 \\ 0.1629$	$\frac{2}{2}$	2 6	1.299E-04 5.775E-04	2 ce . 2 Do	117914.80	123097.63	2	2	1.680E-02
05 7 01	76665.35	113976.72	$\tilde{2}$	4	3.851E-04	$e^2 S^e o s^2 P^o$	$0.1270 \\ 117914.80$	0.0621 125033.70	$\frac{2}{2}$	6 4	2.042E-03 1.362E-03
	76665.35	113962.08	2	2	1.925 E-04		117914.80	125024.90	$\bar{2}$	$\dot{\hat{2}}$	6.800E-04
$b^2S^e o v^2P^o$	0.5028	0.1147	2	6	2.036E-02	$e^2S^e \rightarrow r^2P^o$	0.1270	0.0510	2	6	1.309E-02
	76665.35 76665.35	$\begin{array}{c} 119273.81 \\ 119245.22 \end{array}$	$\frac{2}{2}$	4 2	1.358E-02 6.784E-03		117914.80	126236.40	$\frac{2}{2}$	$\frac{4}{2}$	8.712E-03 4.378E-03
$b^2S^e \rightarrow u^2P^o$	0.5028	0.0939	2	6	5.427E-02	$e^2 S^e \rightarrow q^2 P^o$	$117914.80 \\ 0.1270$	126279.00 0.0484	2	6	7.692E-03
	76665.35	121590.19	2	4	3.622E-02	0 0 7 4 1	117914.80	126525.80	$\tilde{2}$	4	5.124E-03
12.00 .2.00	76665.35	121444.12	2	2	1.805E-02		117914.80	126545.40	2	2	2.568E-03
$b^2S^e \to t^2P^o$	0.5028 76665.35	$0.0795 \\ 123138.67$	$\frac{2}{2}$	6 4	1.035E-02 6.903E-03	$f^2S^e \rightarrow t^2P^o$	0.0914	0.0795	2	6	3.248E+00
	76665.35	123097.63	$\frac{2}{2}$	2	3.448E-03		121814.38 121814.38	$\begin{array}{c} 123138.67 \\ 123097.63 \end{array}$	$\frac{2}{2}$	$\frac{4}{2}$	2.188E+00 1.060E+00
$b^2S^e ightarrow s^2P^o$	0.5028	0.0621	2	6	9.083E-03	$f^2S^e \rightarrow s^2P^o$	0.0914	0.0621	$\bar{2}$	6	2.762E-02
	76665.35	125033.70	2	4	6.056E-03	•	121814.38	125033.70	2	4	1.843E-02
$b^2S^e \rightarrow r^2P^o$	76665.35 0.5028	125024.90 0.0510	$\frac{2}{2}$	2 6	3.027E-03 6.208E-02	$f^2S^e \rightarrow r^2P^o$	121814.38	125024.90	2	2	9.191E-03
0571	76665.35	126236.40	2	4	4.138E-02	$J^{-}S^{\circ} \rightarrow r^{-}P^{\circ}$	0.0914 121814.38	0.0510 126236.40	$\frac{2}{2}$	6 4	2.874E-02 1.910E-02
	76665.35	126279.00	2	2	$2.071\overline{\mathrm{E}}$ - 02		121814.38	126279.00	$\tilde{2}$	$\hat{2}$	9.641E-03
$b^2S^e \to q^2P^o$	0.5028	0.0484	2	6	8.602E-03	$f^2S^e o q^2P^o$	0.0914	0.0484	2	6	2.346E-02
	76665.35 76665.35	$\begin{array}{c} 126525.80 \\ 126545.40 \end{array}$	$\frac{2}{2}$	4 2	5.734E-03 2.868E-03		$\begin{array}{c} 121814.38 \\ 121814.38 \end{array}$	$\frac{126525.80}{126545.40}$	$\frac{2}{2}$	$\frac{4}{2}$	1.562E-02 7.840E-03
$c^2S^e \rightarrow x^2P^o$	0.3087	0.2549	2	6	1.705E+00	$q^2S^e \rightarrow s^2P^o$	0.0690	0.0621	2	6	3.463E+00
	97972.09	103885.25	2	4	1.139E+00	J = 10 *	124276.70	125033.70	2	4	2.317E+00
-2 ce 2 Do	97972.09	103860.74	2	2	5.669E-01	200 200	124276.70	125024.90	2	2	1.145E+00
$c^2 S^e \to w^2 P^o$	0.3087 97972.09	0.1629 113976.72	$\frac{2}{2}$	6 4	2.977E-04 1.986E-04	$g^2S^e ightarrow r^2P^o$	$0.0690 \\ 124276.70$	0.0510 126236.40	2	6 4	1.017E-01 6.729E-02
	97972.09	113962.08	$\frac{2}{2}$	$\overline{2}$	9.919E-05		124276.70	126279.00	$\frac{2}{2}$	2	3.438E-02
$c^2S^e \rightarrow v^2P^o$	0.3087	0.1147	2	6	1.770E-02	$g^2S^e \rightarrow q^2P^o$	0.0690	0.0484	2	6	1.128E-01
	97972.09	$\begin{array}{c} 119273.81 \\ 119245.22 \end{array}$	$\frac{2}{2}$	$\frac{4}{2}$	1.181E-02 5.896E-03	-	124276.70	126525.80	2	4	7.498E-02
$c^2S^e \rightarrow u^2P^o$	97972.09 0.3087	0.0939	2	6	2.022E-02	$a^2P^e \rightarrow x^2P^o$	$124276.70 \\ 0.4366$	126545.40	2 6	2 6	3.782E-02 2.610E-04
00 / 41	97972.09	121590.19	2	4	1.351E-02	$a \rightarrow x^- F^{-1}$	84004.26	0.2549 103885.25	4	4	2.610E-04 2.168E-04
2 ~ 2 -	97972.09	121444.12	2	2	6.711E-03		84004.26	103860.74	4	2	4.331E-05
$c^2S^e o t^2P^o$	0.3087	0.0795	2	6	2.201E-04		83801.95	103885.25	2	4	8.761E-05
	97972.09 97972.09	$\begin{array}{c} 123138.67 \\ 123097.63 \end{array}$	$\frac{2}{2}$	$\frac{4}{2}$	1.468E-04 7.329E-05	$a^2 P^e \rightarrow w^2 P^o$	83801.95 0.4366	103860.74 0.1629	$\frac{2}{6}$	2 6	1.750E-04 1.828E-03
$c^2S^e \rightarrow s^2P^o$	0.3087	0.0621	2	6	3.427E-04	u 1 → w-r-	84004.26	113976.72	4	4	1.828E-03 1.520E-03
	97972.09	125033.70	2	4	2.285E-04		84004.26	113962.08	4	2	3.039E-04
$c^2S^e \rightarrow r^2P^o$	97972.09	125024.90	2	2	1.142E-04		83801.95	113976.72	2	4	6.122E-04
$c^-S^- \rightarrow r^-P^0$	$0.3087 \\ 97972.09$	0.0510 126236.40	$\frac{2}{2}$	6 4	5.615E-03 3.742E-03	$a^2P^e \rightarrow v^2P^o$	83801.95 0.4366	113962.08 0.1147	2 6	2 6	1.224E-03 2.402E-02
	97972.09	126279.00	$\frac{2}{2}$	2	1.874E-03	w 1 7 0 1	84004.26	119273.81	4	4	1.998E-02

TABLE II. Energies and Oscillator Strengths for Allowed Transitions in Si II See page 189 for Explanation of Tables

sition	$\frac{E_i}{\text{Ry/cm}^{-1}}$	$\frac{E_f}{\mathrm{Ry/cm^{-1}}}$	gi	g_f	f_{if}	-	Transition	$\frac{E_i}{\mathrm{Ry/cm^{-1}}}$	$\frac{E_f}{\mathrm{Ry/cm^{-1}}}$	g_i	g_f
	84004.26	119245.22	4	2	3.993E-03			55325.18	103556.16	6	6
	83801.95 83801.95	$\begin{array}{c} 119273.81 \\ 119245.22 \end{array}$	$\frac{2}{2}$	$\frac{4}{2}$	8.039E-03 1.607E-02		2 De . 2 E0	55309.35	103556.16	4	6
u^2P^o	0.4366	0.0939	6	6	5.030E-02		$a^2D^e o y^2F^o$	$0.6974 \\ 55325.18$	$0.1648 \\ 113760.15$	10 6	14 8
	84004.26	121590.19	4	4	4.189E-02			55325.18	113760.32	6	6
	84004.26 83801.95	121444.12	4 2	2	8.346E-03 1.685E-02		200	55309.35	113760.32	4	6
	83801.95	$121590.19 \\ 121444.12$	2	4 2	3.356E-02		$a^2D^e \to x^2F^o$	$0.6974 \\ 55325.18$	0.1142	10	14
t^2P^o	0.4366	0.0795	6	6	5.818E-03			55325.18	119311.19 119311.34	6 6	8 6
	84004.26	123138.67	4	4	4.842E-03			55309.35	119311.34	4	6
	84004.26 83801.95	123097.63 123138.67	$\frac{4}{2}$	$\frac{2}{4}$	9.673E-04 1.947E-03		$a^2D^e o w^2F^o$	0.6974	0.0838	10	14
	83801.95	123138.67	2	2	3.889E-03			55325.18 55325.18	$\substack{122655.25\\122655.37}$	6 6	8 6
$\rightarrow s^2 P^o$	0.4366	0.0621	6	6	1.451E-03			55309.35	122655.37	4	6
	84004.26	125033.70	4	4	1.207E-03		$a^2D^e \rightarrow v^2F^o$	0.6974	0.0640	10	14
	84004.26 83801.95	$\begin{array}{c} 125024.90 \\ 125033.70 \end{array}$	4 2	2 4	2.414E-04 4.852E-04			55325.18	124822.08	6	8
	83801.95	125024.90	$\bar{2}$	$\hat{2}$	9.702E-04			55325.18 55309.35	$\begin{array}{c} 124822.14 \\ 124822.14 \end{array}$	$\frac{6}{4}$	6 6
$\rightarrow r^2 P^o$	0.4366	0.0510	6	6	1.241E-05		$a^2D^e \rightarrow u^2F^o$	0.6974	0.0505	10	14
	84004.26 84004.26	$\begin{array}{c} 126236.40 \\ 126279.00 \end{array}$	4 4	$\frac{4}{2}$	1.032E-05 2.066E-06			55325.18	126304.82	6	8
	83801.95	126236.40	2	4	4.147E-06			55325.18 55309.35	$\begin{array}{c} 126304.82 \\ 126304.82 \end{array}$	6 4	6 6
0	83801.95	126279.00	2	2	8.303E-06		$a^2D^e \rightarrow t^2F^o$	0.6974	0.0408	10	14
$\rightarrow q^2 P^o$	0.4366	0.0484	6	6	9.544E-04		u D 7 (1	55325.18	127363.50	6	8
	84004.26 84004.26	$\begin{array}{c} 126525.80 \\ 126545.40 \end{array}$	4 4	$\frac{4}{2}$	7.940E-04 1.589E-04			55325.18	127363.50	6	6
	83801.95	126525.80	2	4	3.191E-04		$b^2D^e \rightarrow y^2P^o$	55309.35 0.4784	127363.50	4 10	6 6
0	83801.95	126545.40	2	2	6.385E-04		$0D \rightarrow yF$	79355.02	$0.4612 \\ 81251.32$	6	4
$\rightarrow z^2 D^o$	0.4366	$0.2100 \\ 108820.60$	6	10	6.256E-06			79338.50	81251.32	4	4
	84004.26 84004.26	108778.70	4 4	6 4	5.619E-06 6.233E-07		12 00 2 00	79338.50	81191.34	4	2
	83801.95	108778.70	$\hat{2}$	$\hat{4}$	6.284E-06		$b^2D^e \to x^2P^o$	$0.4784 \\ 79355.02$	$0.2549 \\ 103885.25$	$^{10}_{6}$	6 4
y^2P^o	0.6974	0.4612	10	6	5.745×-02			79338.50	103885.25	4	4
	55325.18 55309.35	$81251.32 \\ 81251.32$	6	4 4	5.748E-02 9.585E-03			79338.50	103860.74	4	2
	55309.35	81191.34	4 4	2	4.781E-02		$b^2D^e o w^2P^o$	0.4784	0.1629	10	6
x^2P^o	0.6974	0.2549	10	6	1.007E-02			79355.02 79338.50	$\begin{array}{c} 113976.72 \\ 113976.72 \end{array}$	6 4	4 4
	55325.18	103885.25	6	4	1.007E-02			79338.50	113962.08	4	2
	55309.35 55309.35	$\begin{array}{c} 103885.25 \\ 103860.74 \end{array}$	4 4	$\frac{4}{2}$	1.679E-03 8.389E-03		$b^2D^e ightarrow v^2P^o$	0.4784	0.1147	10	6
w^2P°	0.6974	0.1629	10	6	9.974E-03			79355.02 79338.50	$\begin{array}{c} 119273.81 \\ 119273.81 \end{array}$	6 4	4 4
	55325.18	113976.72	6	4	9.974E-03			79338.50	119245.22	4	2
	55309.35 55309.35	$\begin{array}{c} 113976.72 \\ 113962.08 \end{array}$	4 4	4 2	1.663E-03 8.312E-03		$b^2D^e ightarrow u^2P^o$	0.4784	0.0939	10	6
v^2P^o	0.6974	0.1147	10	6	4.209E-02			79355.02	121590.19	6	4
• 1	55325.18	119273.81	6	4	4.209E-02			79338.50 79338.50	$\begin{array}{c} 121590.19 \\ 121444.12 \end{array}$	4 4	4 2
	55309.35	119273.81	4	4	7.016E-03		$b^2D^e \rightarrow t^2P^o$	0.4784	0.0795	10	6
u^2P^o	55309.35 0.6974	119245.22 0.0939	4 10	2 6	3.507E-02 6.193E-02			79355.02	123138.67	6	4
u 1	55325.18	121590.19	6	4	6.197E-02			79338.50 79338.50	$\begin{array}{c} 123138.67 \\ 123097.63 \end{array}$	4 4	$\frac{4}{2}$
	55309.35	121590.19	4	4	1.033E-02		$b^2D^e \rightarrow s^2P^o$	0.4784	0.0621	10	6
(2.70)	55309.35	121444.12	4	2	5.154E-02		02 ,01	79355.02	125033.70	6	4
t^2P^o	$0.6974 \\ 55325.18$	$0.0795 \\ 123138.67$	10 6	6 4	6.514E-03 6.515E-03			79338.50	125033.70	4	4
	55309.35	123138.67	$\overset{\circ}{4}$	4	1.086E-03		$b^2 D^e \rightarrow r^2 P^o$	79338.50 0.4784	$125024.90 \\ 0.0510$	4 10	2 6
2	55309.35	123097.63	4	2	5.427E- 03		0 D 7 1 1	79355.02	126236.40	6	4
$\rightarrow s^2 P^o$	0.6974	0.0621	10	6	6.727E-03			79338.50	126236.40	4	4
	55325.18 55309.35	$\begin{array}{c} 125033.70 \\ 125033.70 \end{array}$	$\frac{6}{4}$	4 4	6.726E-03 1.121E-03		12 De . 2 Do	79338.50	126279.00	4	2
	55309.35	125024.90	4	$\overset{\mathtt{a}}{2}$	5.606E-03		$b^2D^e o q^2P^o$	$0.4784 \\ 79355.02$	0.0484	10 6	6
r^2P^o	0.6974	0.0510	10	6	8.624 E-02			79338.50	$\begin{array}{c} 126525.80 \\ 126525.80 \end{array}$	4	4 4
	55325.18	126236.40	6	4	8.621E-02			79338.50	126545.40	4	2
	55309.35 55309.35	$\begin{array}{c} 126236.40 \\ 126279.00 \end{array}$	4 4	$\frac{4}{2}$	1.437E-02 7.190E-02		$b^2D^e \rightarrow z^2D^o$	0.4784	0.2100	10	10
q^2P^o	0.6974	0.0484	10	6	1.885E-02			79355.02 79355.02	$108820.60 \\ 108778.70$	6 6	6 4
-	55325.18	126525.80	6	4	1.885E-02			79338.50	108820.60	4	6
	55309.35 55309.35	$126525.80 \\ 126545.40$	4 4	4 2	3.142E-03 1.571E-02		12 04 2	79338.50	108778.70	4	4
z^2D^o	0.6974	0.2100	10	10	2.565E-03		$b^2D^e ightarrow z^2F^o$	0.4784	0.2578	10	14
	55325.18	108820.60	6	6	2.394E-03			79355.02 79355.02	103556.03 103556.16	6 6	8 6
	55325.18	108778.70	6	4	1.709E-04			79338.50	103556.16	4	6
	55309.35 55309.35	$\begin{array}{c} 108820.60 \\ 108778.70 \end{array}$	4 4	6 4	2.566E-04 2.308E-03		$b^2 D^e o y^2 F^o$	0.4784	0.1648	10	14
$^2F^o$	0.6974	0.2578	10	14	1.276E-01			79355.02 79355.02	$\begin{array}{c} 113760.15 \\ 113760.32 \end{array}$	6 6	8 6
	55325.18	103556.03	6	8	1.215E-01			79338.50	113760.32	4	6

TABLE II. Energies and Oscillator Strengths for Allowed Transitions in Si II See page 189 for Explanation of Tables

Transition	E_i	E.	<i>a:</i>	- a -	f.,	Transition	E_i	E_f	gi	g_f	f_{if}
	Ry/cm ⁻¹	$\frac{E_f}{\mathrm{Ry/cm^{-1}}}$	gi	g_f	fif		Ry/cm ⁻¹	Ry/cm ⁻¹	<i>3</i> 1	ا د د	
$b^2D^e o x^2F^o$	0.4784	0.1142	10	14	1.698E-02		101024.35	124822.14	6	6	1.551E-03
	79355.02	119311.19	6	8	1.617E-02	$c^2D^e \rightarrow u^2F^o$	$\begin{array}{c} 101023.05 \\ 0.2809 \end{array}$	$124822.14 \\ 0.0505$	4 10	6 14	3.258E-02 1.930E-02
	79355.02 79338.50	119311.34 119311.34	6 4	6 6	8.084E-04 1.698E-02	CD -7 a r	101024.35	126304.82	6	8	1.838E-02
$b^2D^e \rightarrow w^2F^o$	0.4784	0.0838	10	14	5.574E-03		101024.35	126304.82	6	6	9.190E-04
	79355.02	122655.25	6	8	5.307E-03	$c^2D^e \rightarrow t^2F^o$	0.2809	$126304.82 \\ 0.0408$	4 10	$\frac{6}{14}$	1.930E-02 1.246E-02
	79355.02 79338.50	$\substack{122655.37\\122655.37}$	6 4	6 6	2.654E-04 5.575E-03	$c^-D^- \rightarrow \iota^-\Gamma$	101024.35	127363.50	6	8	1.187E-02
$b^2D^e \rightarrow v^2F^o$	0.4784	0.0640	10	14	2.188E-03		101024.35	127363.50	6	6	5.935E-04
	79355.02	124822.08	6	8	2.083E-03	$d^2D^e \rightarrow w^2P^o$	$\begin{array}{c} 101023.05 \\ 0.1773 \end{array}$	$127363.50 \\ 0.1629$	4 10	6 6	1.246E-02 3.760E-01
	79355.02 79338.50	$\begin{array}{c} 124822.14 \\ 124822.14 \end{array}$	6 4	6 6	1.042E-04 2.188E-03	$a \cdot D \rightarrow w \cdot F$	112394.72	113976.72	6	4	3.771E-01
$b^2D^e \rightarrow u^2F^o$	0.4784	0.0505	10	14	9.701E-04		112394.56	113976.72	4	4	6.286E-02
	79355.02	126304.82	6	8	9.238E-04	$d^2D^e \rightarrow v^2P^o$	112394.56 0.1773	$113962.08 \\ 0.1147$	4 10	2 6	3.114E-01 1.193E-02
	79355.02 79338.50	$\frac{126304.82}{126304.82}$	6 4	6 6	4.619E-05 9.703E-04	a D -701	112394.72	119273.81	6	4	1.195E-02
$b^2D^e \rightarrow t^2F^o$	0.4784	0.0408	10	14	4.726E-04		112394.56	119273.81	4	4 2	1.992E-03
	79355.02	127363.50	6	8	4.500E-04	$d^2D^e \rightarrow u^2P^o$	$\begin{array}{c} 112394.56 \\ 0.1773 \end{array}$	119245.22 0.0939	4 10	6	9.917E-03 2.727E-02
	79355.02 79338.50	$\begin{array}{c} 127363.50 \\ 127363.50 \end{array}$	6 4	6 6	2.250E-05 4.727E-04	4 D 7 4 I	112394.72	121590.19	6	4	2.741E-02
$c^2D^e \rightarrow x^2P^o$	0.2809	0.2549	10	6	2.432E-01		112394.56 112394.56	121590.19 121444.12	4 4	4 2	4.569E-03 2.248E-02
	$\begin{array}{c} 101024.35 \\ 101023.05 \end{array}$	$\begin{array}{c} 103885.25 \\ 103885.25 \end{array}$	6 4	4 4	2.438E-01 4.066E-02	$d^2D^e \rightarrow t^2P^o$	0.1773	0.0795	10	6	2.615E-03
	101023.05	103860.74	4	2	2.016E-01		112394.72	123138.67	6	4	2.618E-03
$c^2D^e \rightarrow w^2P^o$	0.2809	0.1629	10	6	8.736E-04		$\begin{array}{c} 112394.56 \\ 112394.56 \end{array}$	$\begin{array}{c} 123138.67 \\ 123097.63 \end{array}$	4 4	$\frac{4}{2}$	4.364E-04 2.174E-03
	$101024.35 \\ 101023.05$	$\begin{array}{c} 113976.72 \\ 113976.72 \end{array}$	6 4	4 4	8.739E-04 1.457E-04	$d^2D^e \rightarrow s^2P^o$	0.1773	0.0621	10	6	4.158E-04
	101023.05	113962.08	4	2	7.275E-04		112394.72	125033.70	6	4	4.159E-04
$c^2D^e \rightarrow v^2P^o$	0.2809	0.1147	10	6	7.266E-03		$\begin{array}{c} 112394.56 \\ 112394.56 \end{array}$	$\begin{array}{c} 125033.70 \\ 125024.90 \end{array}$	4 4	$\frac{4}{2}$	6.931E-05 3.463E-04
	$101024.35 \\ 101023.05$	$\begin{array}{c} 119273.81 \\ 119273.81 \end{array}$	6 4	4 4	7.270E-03 1.212E-03	$d^2D^e \rightarrow r^2P^o$	0.1773	0.0510	10	6	6.854 E-04
	101023.05	119245.22	4	$\hat{2}$	6.049E-03		$\begin{array}{c} 112394.72 \\ 112394.56 \end{array}$	$\begin{array}{c} 126236.40 \\ 126236.40 \end{array}$	6 4	4 4	6.847E-04 1.141E-04
$c^2D^e o u^2P^o$	0.2809	0.0939 121590.19	10	6	1.278E-02		112394.56	126279.00	4	2	5.723E-04
	$\begin{array}{c} 101024.35 \\ 101023.05 \end{array}$	121590.19	6 4	4 4	1.281E-02 2.135E-03	$d^2D^e o q^2P^o$	0.1773	0.0484	10	6	1.005E-03
200 200	101023.05	121444.12	4	2	1.060E-02		$\begin{array}{c} 112394.72 \\ 112394.56 \end{array}$	$\begin{array}{c} 126525.80 \\ 126525.80 \end{array}$	6 4	4 4	1.004E-03 1.674E-04
$c^2D^e o t^2P^o$	$0.2809 \\ 101024.35$	$0.0795 \\ 123138.67$	10 6	6 4	1.081E-03 1.081E-03		112394.56	126545.40	4	2	8.382E-04
	101023.05	123138.67	4	4	1.802E-04	$d^2D^e o y^2F^o$	0.1773	$0.1648 \\ 113760.15$	10	$^{14}_{8}$	5.414E-01 5.155E-01
$c^2D^e \rightarrow s^2P^o$	101023.05	123097.63	4	2	8.995E-04		$\begin{array}{c} 112394.72 \\ 112394.72 \end{array}$	113760.13	6 6	6	2.578E-02
$cD \rightarrow s^*F$	$0.2809 \\ 101024.35$	0.0621 125033.70	10 6	6 4	1.540E-04 1.540E-04		112394.56	113760.32	4	6	5.414E-01
	101023.05	125033.70	4	4	2.566 E-05	$d^2D^e o x^2F^o$	$0.1773 \\ 112394.72$	0.1142 119311.19	10 6	14 8	3.840E-01 3.658E-01
$c^2D^e \rightarrow r^2P^o$	$\frac{101023.05}{0.2809}$	125024.90 0.0510	4 10	2 6	1.283E-04 1.893E-04		112394.72	119311.34	6	6	1.829E-02
CD 7/1	101024.35	126236.40	6	4	1.892E-04	12 De . 2 Do	112394.56	119311.34	4	6	3.841E-01
	101023.05	126236.40	4	4	3.153E-05	$d^2D^e \rightarrow w^2F^o$	$0.1773 \\ 112394.72$	$0.0838 \\ 122655.25$	$^{10}_{6}$	14 8	1.331E-01 1.268E-01
$c^2D^e \rightarrow g^2P^o$	$\begin{array}{c} 101023.05 \\ 0.2809 \end{array}$	126279.00 0.0484	4 10	$\frac{2}{6}$	1.579E-04 2.982E-04		112394.72	122655.37	6	6	6.340E-03
020 741	101024.35	126525.80	6	4	2.981E-04	$d^2D^e \rightarrow v^2F^o$	112394.56 0.1773	$122655.37 \\ 0.0640$	4 10	6 14	1.331E-01 6.327E-02
	101023.05 101023.05	$\begin{array}{c} 126525.80 \\ 126545.40 \end{array}$	4 4	$\frac{4}{2}$	4.969E-05		112394.72	124822.08	6	8	6.026E-02
$c^2D^e \rightarrow z^2D^o$	0.2809	0.2100	10	10	2.487E-04 9.745E-06		112394.72	124822.14	6	6	3.013E-03
	101024.35	108820.60	6	6	9.114E-06	$d^2D^e \rightarrow u^2F^o$	$112394.56 \\ 0.1773$	$\begin{array}{c} 124822.14 \\ 0.0505 \end{array}$	4 10	$\begin{array}{c} 6 \\ 14 \end{array}$	6.327E-02 3.574E-02
	101024.35 101023.05	$108778.70 \\ 108820.60$	6 4	4 6	6.475E-07 9.767E-07	42 ,41	112394.72	126304.82	6	8	3.404E-02
	101023.05	108778.70	4	4	8.743E-06		$\begin{array}{c} 112394.72 \\ 112394.56 \end{array}$	$\begin{array}{c} 126304.82 \\ 126304.82 \end{array}$	6 4	6 6	1.702E-03 3.574E-02
$c^2D^e \rightarrow z^2F^o$	0.2809	0.2578	10	14	2.782E-01	$d^2D^e \rightarrow t^2F^o$	0.1773	0.0408	10	14	2.255E-02
	$\begin{array}{c} 101024.35 \\ 101024.35 \end{array}$	103556.03 103556.16	6 6	8 6	2.649E-01 1.324E-02		112394.72	127363.50	6	8	2.148E-02
	101023.05	103556.16	4	6	2.783E-01		$\begin{array}{c} 112394.72 \\ 112394.56 \end{array}$	$\begin{array}{c} 127363.50 \\ 127363.50 \end{array}$	$\frac{6}{4}$	6 6	1.074E-03 2.255E-02
$c^2D^e o y^2F^o$	$0.2809 \\ 101024.35$	0.1648	10	14	5.026E-01 4.786E-01	$e^2D^e ightarrow v^2P^o$	0.1214	0.1147	10	6	3.102E-01
	101024.35	$\begin{array}{c} 113760.15 \\ 113760.32 \end{array}$	6 6	8 6	2.393E-02		118522.93	119273.81	6	4	3.141E-01
200 200	101023.05	113760.32	4	6	5.026E-01		$\begin{array}{c} 118522.86 \\ 118522.86 \end{array}$	$\begin{array}{c} 119273.81 \\ 119245.22 \end{array}$	4 4	$\frac{4}{2}$	5.236E-02 2.518E-01
$c^2D^e o x^2F^o$	$0.2809 \\ 101024.35$	0.1142 119311.19	10 6	14 8	1.460E-01 1.390E-01	$e^2D^e o u^2P^o$	0.1214	0.0939	10	6	3.987E-01
	101024.35	119311.19	6	6	6.952E-03		$\begin{array}{c} 118522.93 \\ 118522.86 \end{array}$	$121590.19 \\ 121590.19$	$\frac{6}{4}$	4 4	4.051E-01 6.753E-02
2De - 2E0	101023.05	119311.34	4	6	1.460E-01		118522.86	121444.12	4	2	3.216E-01
$c^2D^e o w^2F^o$	$0.2809 \\ 101024.35$	$0.0838 \\ 122655.25$	10 6	14 8	6.215E-02 5.919E-02	$e^2D^e o t^2P^o$	0.1214	0.0795	10	6	1.008E-02
	101024.35	122655.37	6	6	2.960E-03		$\begin{array}{c} 118522.93 \\ 118522.86 \end{array}$	$\begin{array}{c} 123138.67 \\ 123138.67 \end{array}$	6 4	4 4	1.011E-02 1.685E-03
$c^2D^e \rightarrow v^2F^o$	101023.05	122655.37	4	6	6.216E-02		118522.86	123097.63	4	2	8.348E-03
$c D \rightarrow v^- r^-$	$0.2809 \\ 101024.35$	$0.0640 \\ 124822.08$	10 6	14 8	3.258E-02 3.102E-02	$e^2D^e o s^2P^o$	0.1214	0.0621	10	6	9.194E-04
	- 1.00		•	Ü	J.10211 02						

TABLE II. Energies and Oscillator Strengths for Allowed Transitions in Si II See page 189 for Explanation of Tables

$\begin{array}{c} 118522.93 & 126236.40 & 6 & 4 & 1.819E-03 \\ 118522.86 & 126279.00 & 4 & 2 & 1.524E-03 \\ 0.01214 & 0.0484 & 10 & 6 & 2.166E-03 \\ 118522.93 & 126525.80 & 6 & 4 & 2.164E-03 \\ 118522.86 & 126525.80 & 4 & 4 & 3.606E-04 \\ 118522.86 & 126525.80 & 4 & 4 & 3.606E-04 \\ 118522.86 & 126525.80 & 4 & 2 & 1.808E-03 \\ 0.1214 & 0.1142 & 10 & 14 & 7.512E-01 \\ 118522.93 & 119311.19 & 6 & 8 & 7.152E-01 \\ 118522.93 & 119311.34 & 6 & 6 & 3.577E-02 \\ 118522.93 & 119311.34 & 6 & 6 & 3.577E-02 \\ 118522.93 & 112655.25 & 6 & 8 & 3.048E-01 \\ 118522.93 & 122655.37 & 6 & 6 & 1.524E-02 \\ 118522.93 & 122655.37 & 4 & 6 & 3.200E-01 \\ 118522.93 & 122655.37 & 4 & 6 & 3.200E-01 \\ 118522.93 & 124822.08 & 6 & 8 & 1.132E-01 \\ 118522.93 & 124822.08 & 6 & 8 & 1.132E-01 \\ 118522.93 & 124822.14 & 4 & 6 & 1.188E-01 \\ 118522.93 & 124822.14 & 4 & 6 & 1.188E-01 \\ 118522.93 & 126304.82 & 6 & 8 & 5.642E-02 \\ 118522.93 & 126304.82 & 6 & 6 & 2.821E-03 \\ 118522.93 & 126304.82 & 6 & 6 & 2.821E-03 \\ 118522.93 & 127363.50 & 6 & 6 & 3.305E-02 \\ 118522.93 & 127363.50 & 6 & 6 & 1.652E-03 \\ 118522.93 & 127363.50 & 6 & 6 & 1.652E-03 \\ 118522.93 & 127363.50 & 6 & 6 & 8.0305E-02 \\ 118522.93 & 127363.50 & 6 & 6 & 8.0305E-02 \\ 118522.93 & 127363.50 & 6 & 6 & 8.625E-01 \\ 122163.48 & 123138.67 & 4 & 4 & 1.458E-01 \\ 122163.48 & 123138.67 & 4 & 4 & 1.458E-01 \\ 122163.48 & 123037.03 & 4 & 4 & 6.887E-04 \\ 122163.48 & 122633.70 & 6 & 4 & 4.132E-03 \\ 122163.48 & 122633.70 & 6 & 4 & 4.132E-03 \\ 122163.48 & 122633.80 & 6 & 4 & 5.966E-03 \\ 122163.48 & 122633.70 & 6 & 4 & 4.132E-03 \\ 122163.48 & 122655.25 & 6 & 8 & 8.08E-03 \\ 122163.48 & 12655.37 & 6 & 6 & 4.447E-02 \\ 122163.54 & 122655.25 & 6 & 8 & 8.08E-03 \\ 122163.48 & 12655.37 & 6 & 6 & 4.447E-02 \\ 122163.54 & 122655.37 & 6 & 6 & 4.447E-02 \\ 122163.48 & 12655.37 & 6 & 6 & 4.447E-02 \\ 122163.48 & 12655.37 & 6 & 6 & 4.447E-02 \\ 122163.48 & 12655.37 & 6 & 6 & 4.447E-02 \\ 122163.48 & 12655.37 & 6 & 6 & 4.447E-02 \\ 122163.54 & 12655.57 & 6 & 6 & 4.447E-02 \\ 122163.54 & 122655.57 & 6 & 6 & 4.447E-02 \\ 122163.54 & 12655.57 & 6 & 6 &$						
$ \begin{array}{c} 118522.93 & 125033.70 & 6 & 4 & 9.198E-04 \\ 118522.86 & 125033.70 & 4 & 4 & 1.533E-04 \\ 118522.86 & 125033.70 & 4 & 4 & 1.533E-04 \\ 118522.86 & 125033.70 & 6 & 4 & 9.198E-04 \\ 118522.86 & 126503.70 & 4 & 4 & 1.533E-04 \\ 118522.86 & 126236.40 & 6 & 4 & 1.819F-03 \\ 118522.86 & 126236.40 & 6 & 4 & 1.819F-03 \\ 118522.86 & 126236.40 & 4 & 4 & 3.032E-04 \\ 118522.86 & 126235.80 & 6 & 4 & 2.164E-03 \\ 118522.85 & 126525.80 & 6 & 4 & 2.164E-03 \\ 118522.86 & 126525.80 & 6 & 4 & 2.164E-03 \\ 118522.86 & 126525.80 & 6 & 4 & 2.164E-03 \\ 118522.86 & 126525.80 & 6 & 4 & 2.164E-03 \\ 118522.86 & 126525.80 & 6 & 4 & 2.164E-03 \\ 118522.93 & 119311.9 & 6 & 6 & 7.513E-01 \\ 118522.93 & 119311.9 & 6 & 6 & 7.513E-01 \\ 118522.93 & 119311.34 & 6 & 6 & 3.577E-02 \\ 118522.93 & 112525.25 & 6 & 6 & 1.524E-02 \\ 118522.93 & 12255.25 & 6 & 6 & 3.048E-01 \\ 118522.93 & 12255.25 & 6 & 6 & 3.048E-01 \\ 118522.93 & 12255.25 & 6 & 6 & 1.524E-02 \\ 118522.93 & 12255.25 & 6 & 6 & 1.524E-02 \\ 118522.93 & 124822.08 & 6 & 8 & 1.325E-01 \\ 118522.93 & 124822.08 & 6 & 8 & 1.325E-01 \\ 118522.93 & 124822.14 & 6 & 6 & 5.659E-03 \\ 118522.93 & 126304.82 & 4 & 6 & 5.925E-02 \\ 118522.93 & 126304.82 & 4 & 6 & 5.925E-02 \\ 118522.93 & 126304.82 & 4 & 6 & 5.925E-02 \\ 118522.93 & 126304.82 & 4 & 6 & 5.925E-02 \\ 118522.93 & 126304.82 & 4 & 6 & 5.925E-02 \\ 118522.93 & 127363.50 & 6 & 8 & 3.305E-02 \\ 118522.93 & 127363.50 & 6 & 8 & 3.305E-02 \\ 118522.93 & 127363.50 & 6 & 8 & 3.470E-02 \\ 118522.93 & 127363.50 & 6 & 8 & 3.470E-02 \\ 118522.93 & 127363.50 & 6 & 8 & 3.485E-01 \\ 122163.54 & 12233.867 & 4 & 4 & 1.458E-01 \\ 122163.54 & 12233.867 & 4 & 4 & 1.458E-01 \\ 122163.54 & 12233.867 & 4 & 4 & 1.458E-01 \\ 122163.54 & 12233.867 & 4 & 4 & 1.458E-01 \\ 122163.54 & 12233.867 & 4 & 4 & 1.458E-01 \\ 122163.54 & 12233.867 & 4 & 4 & 1.458E-01 \\ 122163.54 & 12263.640 & 4 & 4 & 9.434E-01 \\ 122163.54 & 126304.82 & 6 & 8 & 5.485E-02 \\ 122163.54 & 124630.482 & 6 & 8 & 5.485E-02 \\ 122163.54 & 122633.70 & 4 & 4 & 1.35E-01 \\ 122163.54 & 12263.37 & 4 & 6 & 9.340E-01 \\ 122163.54 & 12263.37 $	Ru		$\frac{E_f}{\text{Ry/cm}^{-1}}$	g_i	g_f	f_{if}
$e^{2}D^{e} \rightarrow r^{2}P^{o} \qquad 0.1214 \qquad 0.0510 \qquad 10 \qquad 6 \qquad 1.822E-03 \\ 118522.86 \qquad 126236.40 \qquad 6 \qquad 4 \qquad 4 \qquad 3.032E-04 \\ 118522.86 \qquad 126236.40 \qquad 6 \qquad 4 \qquad 4 \qquad 3.032E-04 \\ 118522.86 \qquad 126236.40 \qquad 6 \qquad 4 \qquad 4 \qquad 3.032E-04 \\ 118522.86 \qquad 126236.40 \qquad 6 \qquad 4 \qquad 2 \qquad 1.154E-03 \\ 118522.86 \qquad 126252.80 \qquad 6 \qquad 4 \qquad 2 \qquad 1.154E-03 \\ 118522.86 \qquad 126252.80 \qquad 6 \qquad 4 \qquad 2 \qquad 1.64E-03 \\ 118522.86 \qquad 126525.80 \qquad 6 \qquad 4 \qquad 2 \qquad 1.64E-03 \\ 118522.86 \qquad 126525.80 \qquad 6 \qquad 4 \qquad 2 \qquad 1.64E-03 \\ 118522.86 \qquad 126525.80 \qquad 4 \qquad 4 \qquad 3.606E-04 \\ 118522.86 \qquad 126525.80 \qquad 4 \qquad 4 \qquad 3.606E-04 \\ 118522.86 \qquad 126525.80 \qquad 4 \qquad 4 \qquad 3.606E-04 \\ 118522.86 \qquad 126525.80 \qquad 4 \qquad 4 \qquad 3.606E-04 \\ 118522.93 \qquad 119311.99 \qquad 6 \qquad 8 \qquad 7.153E-01 \\ 118522.93 \qquad 119311.99 \qquad 6 \qquad 8 \qquad 7.153E-01 \\ 118522.93 \qquad 119311.34 \qquad 6 \qquad 6 \qquad 3.577E-02 \\ 118522.93 \qquad 112655.25 \qquad 6 \qquad 6 \qquad 8 \qquad 3.048E-01 \\ 118522.93 \qquad 122655.25 \qquad 6 \qquad 6 \qquad 8 \qquad 3.048E-01 \\ 118522.93 \qquad 122655.25 \qquad 6 \qquad 6 \qquad 8 \qquad 3.048E-01 \\ 118522.93 \qquad 122655.25 \qquad 6 \qquad 6 \qquad 8 \qquad 3.048E-01 \\ 118522.93 \qquad 122655.25 \qquad 6 \qquad 6 \qquad 8 \qquad 3.048E-01 \\ 118522.93 \qquad 122655.25 \qquad 6 \qquad 6 \qquad 8 \qquad 3.00E-01 \\ 118522.93 \qquad 122655.25 \qquad 6 \qquad 6 \qquad 8 \qquad 3.00E-01 \\ 118522.93 \qquad 122655.25 \qquad 6 \qquad 6 \qquad 8 \qquad 3.00E-01 \\ 118522.93 \qquad 122655.25 \qquad 6 \qquad 6 \qquad 8 \qquad 3.00E-01 \\ 118522.93 \qquad 122655.25 \qquad 6 \qquad 6 \qquad 8 \qquad 3.00E-01 \\ 118522.93 \qquad 124822.14 \qquad 6 \qquad 6 \qquad 6 \qquad 5.659E-03 \\ 118522.93 \qquad 124822.14 \qquad 6 \qquad 6 \qquad 6 \qquad 5.659E-03 \\ 118522.93 \qquad 126304.82 \qquad 6 \qquad 6 \qquad 8 \qquad 5.642E-02 \\ 118522.93 \qquad 127363.50 \qquad 6 \qquad 6 \qquad 8 \qquad 5.642E-02 \\ 118522.93 \qquad 127363.50 \qquad 6 \qquad 6 \qquad 8 \qquad 5.642E-02 \\ 118522.93 \qquad 127363.50 \qquad 6 \qquad 6 \qquad 8 \qquad 8.255E-02 \\ 122163.48 \qquad 123138.67 \qquad 6 \qquad 4 \qquad 4 \qquad 1.458E-01 \\ 122163.48 \qquad 123138.67 \qquad 6 \qquad 4 \qquad 4 \qquad 1.458E-01 \\ 122163.48 \qquad 123138.67 \qquad 6 \qquad 4 \qquad 4 \qquad 1.458E-01 \\ 122163.48 \qquad 123138.67 \qquad 6 \qquad 4 \qquad 4 \qquad 1.458E-01 \\ 122163.48 \qquad 12363.40 \qquad 6 \qquad 4 \qquad 4 \qquad 9.943E-04 \\ 122163.48 \qquad 123636.40 \qquad 6 \qquad 4 \qquad 4 \qquad 9.943E-04 \\ 122163.48 \qquad 12636.40 \qquad 6 \qquad 4 \qquad 4 \qquad 9.943E-04 \\ 122163.48 \qquad 126253.00 \qquad 6 \qquad 6 \qquad 6 \qquad 5.986E-03 \\ 122163.48 \qquad 126253.00 \qquad 6 \qquad 6 \qquad 6 \qquad 5.986E-03 \\ 122163.48 \qquad 126253.00 \qquad 6 \qquad 6 \qquad 6 \qquad 5.986E-03 \\ 122163.48 \qquad 126253.00 \qquad 6 \qquad 6 \qquad 6 \qquad 5.86E-03 \\ 12$				6		0 109E 04
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$\begin{array}{c} 1 8522.86 & 126236.40 & 4 & 4 & 3.032E-04 \\ 1 8522.86 & 126279.00 & 4 & 2 & 1.524E-03 \\ 0.1214 & 0.0484 & 10 & 6 & 2.166E-03 \\ 1 8522.86 & 126525.80 & 4 & 4 & 3.606E-04 \\ 1 8522.86 & 126525.80 & 4 & 4 & 3.606E-04 \\ 1 8522.86 & 126525.80 & 4 & 4 & 3.606E-04 \\ 1 8522.86 & 126525.80 & 4 & 4 & 3.606E-04 \\ 1 8522.93 & 119311.91 & 0 & 14 & 7.512E-01 \\ 1 8522.93 & 119311.34 & 6 & 6 & 3.577E-02 \\ 1 8522.93 & 119311.34 & 6 & 6 & 3.577E-02 \\ 1 8522.93 & 12655.25 & 6 & 8 & 3.048E-01 \\ 1 8522.93 & 122655.25 & 6 & 8 & 3.048E-01 \\ 1 8522.93 & 122655.37 & 6 & 6 & 1.524E-02 \\ 1 8522.93 & 122855.37 & 6 & 6 & 1.524E-02 \\ 1 8522.93 & 124852.80 & 6 & 8 & 1.132E-01 \\ 1 8522.93 & 124852.80 & 6 & 8 & 1.132E-01 \\ 1 8522.93 & 124852.80 & 6 & 8 & 1.132E-01 \\ 1 8522.93 & 124852.90 & 6 & 8 & 1.132E-01 \\ 1 8522.93 & 124852.90 & 6 & 8 & 1.132E-01 \\ 1 8522.93 & 124852.90 & 6 & 8 & 1.132E-01 \\ 1 8522.93 & 124852.00 & 6 & 8 & 1.132E-01 \\ 1 8522.93 & 124852.00 & 6 & 8 & 1.132E-01 \\ 1 8522.93 & 124852.00 & 6 & 8 & 1.132E-01 \\ 1 8522.93 & 124852.00 & 6 & 8 & 2.42E-02 \\ 1 8522.93 & 126304.82 & 6 & 6 & 2.821E-03 \\ 1 8522.93 & 127630.82 & 6 & 6 & 2.821E-03 \\ 1 8522.93 & 127630.82 & 6 & 6 & 2.821E-03 \\ 1 8522.93 & 127363.80 & 6 & 6 & 3.305E-02 \\ 1 8522.93 & 127363.80 & 6 & 6 & 1.652E-03 \\ 1 8522.93 & 127363.80 & 6 & 6 & 1.652E-03 \\ 1 8522.93 & 127363.80 & 6 & 6 & 1.652E-03 \\ 1 8522.93 & 127363.80 & 6 & 6 & 1.652E-03 \\ 1 8522.93 & 127363.80 & 6 & 6 & 1.652E-03 \\ 1 8522.93 & 127363.80 & 6 & 6 & 1.652E-03 \\ 1 8522.93 & 127363.80 & 6 & 6 & 1.652E-03 \\ 1 8522.93 & 127363.80 & 6 & 6 & 1.652E-03 \\ 1 8522.93 & 127363.80 & 6 & 6 & 1.652E-03 \\ 1 8522.93 & 127363.80 & 6 & 6 & 1.652E-03 \\ 1 8522.93 & 127363.80 & 6 & 6 & 1.652E-03 \\ 1 8522.93 & 127363.80 & 6 & 6 & 1.652E-03 \\ 1 8522.93 & 127363.80 & 6 & 6 & 1.652E-03 \\ 1 22163.54 & 12233.807 & 6 & 4 & 4.748E-01 \\ 1 22163.54 & 12233.807 & 6 & 4 & 4.748E-01 \\ 1 22163.54 & 12263.80 & 4 & 6 & 5.852E-03 \\ 1 22163.54 & 12263.80 & 4 & 4 & 5.858E-03 \\ 1 22163.54 & 12263.80 & 6 & 6 & 5.852E-03 \\ 1 22163.54 & 12263.$	113					
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$e^2D^c \to x^2F^o \\ 118852.93 & 119311.99 & 6 & 8 & 7.153E-01 \\ 118852.93 & 119311.34 & 6 & 6 & 3.577E-02 \\ 118852.93 & 119311.34 & 6 & 6 & 3.577E-02 \\ 118852.93 & 112631.34 & 6 & 6 & 3.577E-02 \\ 118852.93 & 122655.25 & 6 & 8 & 3.048E-01 \\ 118852.93 & 122655.25 & 6 & 8 & 3.048E-01 \\ 118852.93 & 122655.37 & 6 & 6 & 1.524E-02 \\ 118852.93 & 122655.37 & 6 & 6 & 1.524E-02 \\ 118852.93 & 124822.08 & 6 & 8 & 1.132E-01 \\ 118852.93 & 124822.14 & 6 & 6 & 5.659E-03 \\ 118852.93 & 124822.14 & 6 & 6 & 5.659E-03 \\ 118852.93 & 124822.14 & 6 & 6 & 5.659E-03 \\ 118852.93 & 124822.14 & 6 & 6 & 5.659E-03 \\ 118852.93 & 126304.82 & 6 & 8 & 5.642E-02 \\ 118852.93 & 126304.82 & 6 & 6 & 2.821E-03 \\ 118852.93 & 126304.82 & 6 & 6 & 2.821E-03 \\ 118852.93 & 127363.50 & 6 & 8 & 3.059E-02 \\ 118852.93 & 127363.50 & 6 & 8 & 3.059E-02 \\ 118852.93 & 127363.50 & 6 & 8 & 3.059E-02 \\ 118852.93 & 127363.50 & 6 & 8 & 8.625E-01 \\ 122163.48 & 123038.67 & 6 & 4 & 8.748E-01 \\ 122163.48 & 12303.70 & 6 & 4 & 8.748E-01 \\ 122163.48 & 12303.70 & 6 & 4 & 4.128E-03 \\ 122163.48 & 125033.70 & 6 & 4 & 4.128E-03 \\ 122163.48 & 125033.70 & 6 & 4 & 4.128E-03 \\ 122163.48 & 125033.70 & 6 & 4 & 4.128E-03 \\ 122163.48 & 125033.70 & 6 & 4 & 4.128E-03 \\ 122163.48 & 125033.70 & 6 & 4 & 4.128E-03 \\ 122163.48 & 125033.70 & 6 & 4 & 4.128E-03 \\ 122163.48 & 126356.40 & 6 & 4 & 5.966E-03 \\ 122163.48 & 126356.40 & 6 & 4 & 5.966E-03 \\ 122163.48 & 126356.40 & 6 & 4 & 5.966E-03 \\ 122163.48 & 126356.40 & 6 & 4 & 5.966E-03 \\ 122163.48 & 126356.40 & 6 & 4 & 5.966E-03 \\ 122163.48 & 126356.40 & 6 & 4 & 5.966E-03 \\ 122163.48 & 126356.40 & 6 & 4 & 5.966E-03 \\ 122163.48 & 126356.40 & 6 & 4 & 5.966E-03 \\ 122163.48 & 126356.40 & 6 & 4 & 5.966E-03 \\ 122163.48 & 126356.40 & 6 & 4 & 5.966E-03 \\ 122163.48 & 126356.40 & 6 & 4 & 5.966E-03 \\ 122163.48 & 126356.40 & 6 & 4 & 5.966E-03 \\ 122163.48 & 126356.40 & 6 & 4 & 5.966E-03 \\ 122163.48 & 126356.40 & 6 & 4 & 5.966E-03 \\ 122163.48 & 126356.40 & 6 & 4 & 5.966E-03 \\ 122163.48 & 126356.40 & 6 & 6 & 5.986E-03 \\ 122163.48 & 126356.40 & 6 & 6 & 5.986E-03 \\ 1221$						
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$\begin{array}{c} 18852.93 & 122655.37 & 6 & 6 & 1.524E.02 \\ 18852.98 & 122655.37 & 6 & 6 & 1.520E.01 \\ 18852.93 & 12482.08 & 6 & 8 & 1.135E.01 \\ 18852.93 & 12482.08 & 6 & 8 & 1.135E.01 \\ 18852.93 & 124822.14 & 6 & 6 & 5.650E.03 \\ 118852.28 & 124822.14 & 6 & 6 & 5.650E.03 \\ 118852.28 & 124822.14 & 6 & 6 & 5.650E.03 \\ 118852.29 & 124822.14 & 6 & 6 & 5.650E.03 \\ 118852.29 & 126304.82 & 6 & 8 & 5.642E.02 \\ 118852.23 & 126304.82 & 6 & 8 & 5.642E.02 \\ 11852.23 & 126304.82 & 6 & 6 & 2.821E.03 \\ 11852.23 & 127363.50 & 6 & 8 & 3.305E.02 \\ 11852.29 & 127363.50 & 6 & 6 & 1.652E.03 \\ 11852.29 & 127363.50 & 6 & 6 & 1.652E.03 \\ 11852.29 & 127363.50 & 6 & 6 & 1.652E.03 \\ 11852.28 & 127363.50 & 6 & 6 & 1.652E.03 \\ 11852.39 & 127363.50 & 6 & 6 & 1.652E.03 \\ 12163.48 & 123138.67 & 6 & 8.748E.01 \\ 122163.48 & 123338.67 & 6 & 8.748E.01 \\ 122163.48 & 123097.63 & 4 & 6.988E.01 \\ 122163.48 & 123097.63 & 4 & 6.988E.01 \\ 122163.48 & 123097.63 & 4 & 6.988E.04 \\ 122163.48 & 123097.63 & 4 & 6.988E.04 \\ 122163.48 & 125024.90 & 4 & 2 & 3.433E.03 \\ 122163.48 & 125024.90 & 4 & 2 & 3.433E.03 \\ 122163.48 & 126026.40 & 6 & 4 & 5.966E.03 \\ 122163.48 & 126026.40 & 6 & 4 & 5.966E.03 \\ 122163.48 & 126026.40 & 6 & 4 & 5.966E.03 \\ 122163.48 & 126025.80 & 6 & 4 & 5.488E.04 \\ 122163.48 & 126055.80 & 6 & 4 & 5.488E.04 \\ 122163.48 & 126055.80 & 6 & 4 & 5.488E.01 \\ 122163.48 & 126055.80 & 6 & 4 & 5.488E.01 \\ 122163.54 & 122655.37 & 6 & 8.892E.01 \\ 122163.54 & 122633.80 & 6 & 8.2682E.01 \\ 122163.54 & 122633.80 & 6 & 8.2682E.01 \\ 122163.54 & 123633.50 & 6 & 8.892E.01 \\ 122163.54 & 12$						
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	11 11	8522.93				
$\begin{array}{cccccccccccccccccccccccccccccccccccc$		8522.86	122655.37			
$\begin{array}{c} 118522.93 & 124822.14 & 6 & 6 & 5.659E.03 \\ 118522.86 & 124822.14 & 6 & 1.188E.01 \\ e^2D^e \to u^2F^o & 0.1214 & 0.0505 & 10 & 14 & 5.925E.02 \\ 118522.93 & 126304.82 & 6 & 6 & 2.821E.03 \\ 118522.93 & 126304.82 & 6 & 6 & 2.821E.03 \\ e^2D^e \to t^2F^o & 0.1214 & 0.0408 & 10 & 14 & 3.470E.02 \\ 118522.93 & 127363.50 & 6 & 8 & 3.305E.02 \\ 118522.93 & 127363.50 & 6 & 6 & 1.652E.03 \\ 118522.93 & 127363.50 & 6 & 6 & 3.470E.02 \\ 118522.93 & 127363.50 & 4 & 6 & 3.470E.02 \\ 118522.93 & 127363.50 & 4 & 6 & 3.470E.02 \\ 12163.54 & 123138.67 & 6 & 4 & 8.748E.01 \\ 122163.48 & 123138.67 & 6 & 4 & 8.748E.01 \\ 122163.48 & 123138.67 & 6 & 4 & 8.748E.01 \\ 122163.48 & 1233097.63 & 4 & 2 & 6.983E.01 \\ f^2D^e \to s^2P^o & 0.0882 & 0.0621 & 10 & 6 & 4.132E.03 \\ 122163.48 & 123037.0 & 6 & 4 & 4.132E.03 \\ 122163.48 & 125033.70 & 6 & 4 & 4.132E.03 \\ 122163.48 & 125033.70 & 6 & 4 & 4.132E.03 \\ 122163.48 & 125033.70 & 6 & 4 & 4.132E.03 \\ 122163.48 & 125033.70 & 6 & 4 & 5.96E.03 \\ 122163.48 & 125034.90 & 4 & 2 & 3.433E.03 \\ f^2D^e \to r^2P^o & 0.0882 & 0.0510 & 10 & 6 & 5.986E.03 \\ 122163.48 & 12636.40 & 6 & 4 & 5.966E.03 \\ 122163.48 & 12653.80 & 6 & 4 & 5.492E.03 \\ 122163.48 & 126525.80 & 6 & 4 & 5.492E.03 \\ 122163.48 & 126525.80 & 6 & 4 & 5.492E.03 \\ 122163.54 & 12655.37 & 6 & 6 & 4.47E.02 \\ 122163.54 & 122655.37 & 6 & 6 & 4.47E.02 \\ 122163.54 & 122655.37 & 6 & 6 & 4.47E.02 \\ 122163.54 & 122655.37 & 6 & 6 & 4.47E.02 \\ 122163.54 & 122655.37 & 6 & 6 & 4.47E.02 \\ 122163.54 & 122655.37 & 6 & 6 & 4.47E.02 \\ 122163.54 & 122655.37 & 6 & 6 & 4.47E.02 \\ 122163.54 & 122655.37 & 6 & 6 & 4.47E.02 \\ 122163.54 & 122655.37 & 6 & 6 & 4.47E.02 \\ 122163.54 & 122655.37 & 6 & 6 & 4.47E.02 \\ 122163.54 & 122655.37 & 6 & 6 & 4.47E.02 \\ 122163.54 & 122655.37 & 6 & 6 & 4.47E.02 \\ 122163.54 & 122655.37 & 6 & 6 & 4.568E.01 \\ f^2D^e \to v^2F^o & 0.0882 & 0.0640 & 10 & 14 & 2.816E.01 \\ f^2D^e \to v^2F^o & 0.0882 & 0.0640 & 10 & 14 & 2.816E.01 \\ f^2D^e \to v^2F^o & 0.0882 & 0.0605 & 10 & 14 & 1.08TE.01 \\ f^2D^e \to v^2F^o & 0.0682 & 0.0606 & 10 & 14 & 5.858E.02 \\ 0.0670 & 0.068$	11					
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	11	8522.93	124822.14	6	6	5.659E-03
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$\begin{array}{cccccccccccccccccccccccccccccccccccc$	11	8522.93	126304.82			2.821E-03
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	11				-	
$\begin{array}{cccccccccccccccccccccccccccccccccccc$		8522.93	127363.50	6	8	3.305E-02
$\begin{array}{cccccccccccccccccccccccccccccccccccc$						
$\begin{array}{c} 122163.48 & 123138.67 & 4 & 4 & 1.488E.01 \\ 122163.48 & 123097.63 & 4 & 2 & 6.983E.01 \\ 122163.48 & 125033.70 & 6 & 4.128E.03 \\ 122163.48 & 125033.70 & 6 & 4.128E.03 \\ 122163.48 & 125033.70 & 4 & 4.6.887E.04 \\ 122163.48 & 125032.490 & 4 & 2 & 3.433E.03 \\ 122163.48 & 125024.90 & 4 & 2 & 3.433E.03 \\ 122163.54 & 126326.40 & 6 & 4 & 5.966E.03 \\ 122163.48 & 126226.40 & 6 & 4 & 5.966E.03 \\ 122163.48 & 126236.40 & 6 & 4 & 5.966E.03 \\ 122163.48 & 126236.40 & 6 & 4 & 5.966E.03 \\ 122163.48 & 126236.40 & 6 & 4 & 5.966E.03 \\ 122163.48 & 126236.40 & 6 & 4 & 5.966E.03 \\ 122163.48 & 126236.40 & 6 & 4 & 5.966E.03 \\ 122163.48 & 126525.80 & 6 & 4 & 5.986E.03 \\ 122163.48 & 126525.80 & 6 & 4 & 5.483E.03 \\ 122163.48 & 126525.80 & 6 & 4 & 5.483E.03 \\ 122163.48 & 126525.80 & 6 & 4 & 5.483E.03 \\ 122163.48 & 126525.80 & 6 & 4 & 5.483E.03 \\ 122163.48 & 126525.80 & 6 & 4 & 5.483E.03 \\ 122163.48 & 126552.57 & 6 & 8 & 8.892E.01 \\ 122163.54 & 122655.37 & 6 & 6 & 4.447E.02 \\ 122163.54 & 122655.37 & 6 & 6 & 4.447E.02 \\ 122163.54 & 122655.37 & 6 & 6 & 4.447E.02 \\ 122163.54 & 122655.37 & 6 & 6 & 4.447E.02 \\ 122163.54 & 122855.37 & 6 & 6 & 4.447E.02 \\ 122163.54 & 122855.37 & 6 & 6 & 1.341E.02 \\ 122163.54 & 124822.14 & 6 & 6 & 1.341E.02 \\ 122163.54 & 124822.14 & 6 & 6 & 1.341E.02 \\ 122163.54 & 124822.14 & 6 & 6 & 1.341E.02 \\ 122163.54 & 126304.82 & 6 & 8 & 1.035E.01 \\ 122163.54 & 126304.82 & 6 & 8 & 1.035E.01 \\ 122163.54 & 126304.82 & 6 & 8 & 1.035E.01 \\ 122163.54 & 126304.82 & 6 & 6 & 5.176E.03 \\ 122163.54 & 122303.70 & 6 & 6 & 5.554E.02 \\ 122163.54 & 127363.50 & 6 & 6 & 5.554E.02 \\ 122163.54 & 127363.50 & 6 & 6 & 5.554E.02 \\ 122163.54 & 127363.50 & 6 & 6 & 5.555E.02 \\ 122163.54 & 127363.50 & 6 & 6 & 5.555E.02 \\ 122163.54 & 127363.50 & 6 & 6 & 5.555E.02 \\ 124495.70 & 125033.70 & 6 & 4 & 9.144E.01 \\ 124495.70 & 126236.40 & 6 & 5.555E.02 \\ 124495.70 & 126236.40 & 6 & 4 & 5.579E.03 \\ 124495.70 & 126236.40 & 6 & 4 & 5.579E.03 \\ 124495.70 & 126236.40 & 6 & 4 & 5.579E.03 \\ 124495.70 & 126236.40 & 6 & 4 & 5.579E.03 \\ 124495.70 & 126236.40 & 6 & $	- 11					
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$\begin{array}{c} 122163.48 & 125033.70 & 4 & 4 & 6.887E-04 \\ 122163.48 & 125024.90 & 4 & 2 & 3.433E-03 \\ 122163.48 & 125024.90 & 4 & 2 & 3.433E-03 \\ 122163.54 & 126236.40 & 6 & 4 & 5.966E-03 \\ 122163.54 & 126236.40 & 6 & 4 & 5.966E-03 \\ 122163.48 & 126279.00 & 4 & 2 & 5.023E-03 \\ 122163.48 & 126279.00 & 4 & 2 & 5.023E-03 \\ 122163.54 & 126525.80 & 6 & 4 & 5.483E-03 \\ 122163.48 & 126525.80 & 6 & 4 & 5.483E-03 \\ 122163.48 & 126525.80 & 4 & 4 & 9.139E-04 \\ 122163.48 & 1265525.80 & 4 & 4 & 9.139E-04 \\ 122163.48 & 126555.55 & 6 & 8 & 8.892E-01 \\ 122163.48 & 126555.55 & 6 & 8 & 8.892E-01 \\ 122163.54 & 122655.37 & 6 & 6 & 4.447E-02 \\ 122163.54 & 122655.37 & 6 & 6 & 4.447E-02 \\ 122163.54 & 122655.37 & 6 & 6 & 4.447E-02 \\ 122163.54 & 124822.08 & 6 & 8 & 2.682E-01 \\ 122163.54 & 124822.08 & 6 & 8 & 2.682E-01 \\ 122163.54 & 124822.14 & 6 & 6 & 1.341E-02 \\ 122163.54 & 124822.14 & 6 & 6 & 1.341E-02 \\ 122163.54 & 124822.14 & 6 & 6 & 1.341E-02 \\ 122163.54 & 124832.08 & 6 & 8 & 1.035E-01 \\ 122163.54 & 124832.08 & 6 & 8 & 1.035E-01 \\ 122163.54 & 124832.08 & 6 & 8 & 1.035E-01 \\ 122163.54 & 124832.08 & 6 & 8 & 1.035E-01 \\ 122163.54 & 126304.82 & 6 & 8 & 1.035E-01 \\ 122163.54 & 126304.82 & 6 & 8 & 1.035E-01 \\ 122163.54 & 126304.82 & 6 & 8 & 1.035E-01 \\ 122163.54 & 126304.82 & 6 & 8 & 1.035E-01 \\ 122163.54 & 126304.82 & 6 & 8 & 1.035E-01 \\ 122163.54 & 127363.50 & 6 & 6 & 2.645E-03 \\ 122163.54 & 127363.50 & 6 & 6 & 2.645E-03 \\ 122163.54 & 127363.50 & 6 & 6 & 2.645E-03 \\ 122163.54 & 127363.50 & 6 & 6 & 2.645E-03 \\ 122163.54 & 127363.50 & 6 & 6 & 2.645E-03 \\ 122163.54 & 127363.50 & 6 & 6 & 2.645E-03 \\ 122163.54 & 127363.50 & 6 & 6 & 2.645E-03 \\ 122163.54 & 127363.50 & 6 & 6 & 2.645E-03 \\ 122163.54 & 127363.50 & 6 & 6 & 2.645E-03 \\ 122163.54 & 127363.50 & 6 & 6 & 2.645E-03 \\ 122163.54 & 127363.50 & 6 & 6 & 2.645E-03 \\ 122163.54 & 127363.50 & 6 & 6 & 2.645E-03 \\ 122163.54 & 127363.50 & 6 & 6 & 2.645E-03 \\ 122163.54 & 127363.50 & 6 & 6 & 2.645E-03 \\ 122163.54 & 127363.50 & 6 & 6 & 2.645E-03 \\ 122163.54 & 127363.50 & 6 & 6 & 2.645E-03 \\ 124495.70 & 12$	• •					
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$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	12	22163.48	125024.90	4	2	3.433E-03
$\begin{array}{c} 122163.48 & 126236.40 & 4 & 4 & 9.943E-04 \\ 122163.48 & 126279.00 & 4 & 2 & 5.023E-03 \\ 0.0882 & 0.0484 & 10 & 6 & 5.492E-03 \\ 122163.48 & 126525.80 & 6 & 4 & 5.483E-03 \\ 122163.48 & 1265525.80 & 6 & 4 & 5.483E-03 \\ 122163.48 & 1265525.80 & 4 & 4 & 9.139E-04 \\ 122163.48 & 1265525.80 & 4 & 4 & 9.139E-04 \\ 122163.54 & 122655.50 & 4 & 4 & 9.139E-04 \\ 122163.54 & 122655.52 & 6 & 8.892E-01 \\ 122163.54 & 122655.57 & 6 & 8.892E-01 \\ 122163.54 & 122655.37 & 6 & 6 & 4.47E-02 \\ 122163.54 & 122655.37 & 6 & 6 & 4.47E-02 \\ 122163.54 & 124822.18 & 6 & 8 & 2.682E-01 \\ 122163.54 & 124822.08 & 6 & 8 & 2.682E-01 \\ 122163.54 & 124822.14 & 6 & 6 & 1.341E-02 \\ 122163.54 & 124822.14 & 6 & 6 & 1.341E-02 \\ 122163.54 & 124822.14 & 6 & 6 & 1.341E-02 \\ 122163.54 & 124822.14 & 6 & 6 & 1.341E-02 \\ 122163.54 & 124822.14 & 6 & 6 & 1.341E-02 \\ 122163.54 & 124822.14 & 6 & 6 & 1.341E-02 \\ 122163.54 & 124822.14 & 6 & 6 & 1.341E-02 \\ 122163.54 & 124820.14 & 6 & 6 & 1.341E-02 \\ 122163.54 & 126304.82 & 6 & 8 & 1.035E-01 \\ 122163.54 & 126304.82 & 6 & 8 & 1.035E-01 \\ 122163.54 & 126304.82 & 6 & 8 & 1.035E-01 \\ 122163.54 & 126304.82 & 6 & 8 & 1.035E-01 \\ 122163.54 & 127363.50 & 6 & 6 & 5.176E-03 \\ 122163.54 & 127363.50 & 6 & 6 & 2.645E-03 \\ 122163.54 & 127363.50 & 6 & 6 & 2.645E-03 \\ 122163.54 & 127363.50 & 6 & 6 & 2.645E-03 \\ 122163.54 & 127363.50 & 6 & 6 & 2.645E-03 \\ 122163.54 & 127363.50 & 6 & 6 & 2.645E-03 \\ 124495.70 & 125033.70 & 4 & 4 & 1.524E-01 \\ 124495.70 & 125033.70 & 4 & 4 & 1.524E-01 \\ 124495.70 & 125033.70 & 4 & 4 & 1.524E-01 \\ 124495.70 & 125033.70 & 4 & 4 & 1.524E-01 \\ 124495.70 & 125033.70 & 4 & 4 & 1.524E-01 \\ 124495.70 & 126236.40 & 6 & 4 & 3.527E-02 \\ 124495.70 & 126236.40 & 6 & 4 & 3.527E-02 \\ 124495.70 & 126236.40 & 6 & 4 & 3.527E-02 \\ 124495.70 & 126236.40 & 6 & 4 & 3.527E-02 \\ 124495.70 & 126236.40 & 6 & 4 & 3.527E-02 \\ 124495.70 & 126236.40 & 6 & 4 & 3.527E-02 \\ 124495.70 & 126236.40 & 6 & 4 & 3.527E-02 \\ 124495.70 & 126236.40 & 6 & 4 & 3.527E-02 \\ 124495.70 & 126236.40 & 6 & 4 & 3.527E-02 \\ 124495.70 & 126236.40 & 6 &$						
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	12	22163.48	126236.40	4	4	9.943E-04
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$\begin{array}{cccccccccccccccccccccccccccccccccccc$						
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$\begin{array}{c} f^2D^e \rightarrow v^2F^o \\ f^2D^$	12	22163.54	122655.25	6	8	8.892E-01
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$\begin{array}{cccccccccccccccccccccccccccccccccccc$		22163.48	126304.82	4	6	1.087 E-01
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$\begin{array}{cccccccccccccccccccccccccccccccccccc$	12					
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$\begin{array}{cccccccccccccccccccccccccccccccccccc$	12	24495.70	125033.70			1.524E-01
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	12					
$g^2D^e \rightarrow q^2P^o \\ \begin{array}{ccccccccccccccccccccccccccccccccccc$	12	24495.70	126236.40	6	4	3.527E-02
$\begin{array}{cccccccccccccccccccccccccccccccccccc$						
124495.70 126525.80 6 4 2.285E-02 $z^2P^3 \rightarrow a^2S^c$ 1.1997	. 12					
124495.7U 126525.8U 4 4 3.8U9E-U3 201.24	12	24495.70	126525.80	6	4	2.285E-02
124495.70 126545.40 4 2 1.923E-02 0.00						

TABLE II. Energies and Oscillator Strengths for Allowed Transitions in Si II See page 189 for Explanation of Tables

Transition	$\frac{E_i}{\mathrm{Ry/cm^{-1}}}$	$rac{E_f}{ m Ry/cm^{-1}}$	g_i	g_f	f_{if}	Transition	E_i Ry/cm ⁻¹	$\frac{E_f}{\mathrm{Ry/cm^{-1}}}$	g_i	g_f	fif
$z^2P^o \rightarrow b^2S^e$	1.1997		c	٠,	8.399E-02	$u^2P^o \rightarrow d^2D^e$	0.4612	0.1773	6	10	1.495E-01
$z \cdot I \rightarrow 0 \cdot S$	287.24	$0.5028 \\ 76665.35$	6 4	$\frac{2}{2}$	8.388E-02	g I , u D	81251.32	112394.72	4	6	1.345E-01
	0.00	76665.35	$\bar{2}$	$\bar{2}$	8.420E-02		81251.32	112394.56	4	4	1.494E-02
$z^2P^o o c^2S^e$	1.1997	0.3087	6	2	1.453E-02	.2 Do2 De	81191.34	112394.56	2	4	1.497E-01
	287.24	97972.09	$\frac{4}{2}$	$\frac{2}{2}$	1.452E-02 1.456E-02	$y^2P^o o e^2D^e$	$0.4612 \\ 81251.32$	0.1214 118522.93	6 4	10 6	4.511E-02 4.057E-02
$z^2P^o \rightarrow d^2S^e$	$0.00 \\ 1.1997$	$97972.09 \\ 0.1883$	6	2	5.584E-03		81251.32	118522.86	4	4	4.508E-03
21 / 4 5	287.24	111184.46	4	$\tilde{2}$	5.579E-03	0	81191.34	118522.86	2	4	4.515E-02
0 0	0.00	111184.46	2	2	5.593E-03	$y^2P^o o f^2D^e$	$0.4612 \\ 81251.32$	0.0882	6	10	1.803E-02
$z^2 P^o \rightarrow e^2 S^e$	$1.1997 \\ 287.24$	0.1270	6	$\frac{2}{2}$	2.794E-03		81251.32	$122163.54 \\ 122163.48$	4	6 4	1.622E-02 1.802E-03
	0.00	$117914.80 \\ 117914.80$	4 2	2	2.791E-03 2.798E-03		81191.34	122163.48	$\tilde{2}$	$\tilde{4}$	1.805E-02
$z^2P^o o f^2S^e$	1.1997	0.0914	$\bar{6}$	$\bar{2}$	1.609E-03	$y^2 P^o o g^2 D^e$	0.4612	0.0670	6	10	8.708E-03
•	287.24	121814.38	4	2	1.607E-03		$81251.32 \\ 81251.32$	$124495.70 \\ 124495.70$	4 4	6 4	7.834E-03 8.704E-04
2 Do . 2 Ge	0.00	121814.38	2	2	1.611E-03		81191.34	124495.70	2	4	8.716E-03
$z^2 P^o o g^2 S^e$	$1.1997 \\ 287.24$	$0.0690 \\ 124276.70$	6 4	$\frac{2}{2}$	1.016E-03 1.016E-03	$x^2P^o \rightarrow d^2S^e$	0.2549	0.1883	6	2	3.278E-01
	0.00	124276.70	2	$\tilde{2}$	1.018E-03		103885.25	111184.46	4	2	3.275E-01
$z^2P^o \rightarrow a^2P^e$	1.1997	0.4366	6	6	8.721E-01	$x^2P^o \rightarrow e^2S^e$	103860.74	111184.46	2	$\frac{2}{2}$	3.286E-01 4.372E-02
	287.24	84004.26	4	4	7.265E-01	$x^-F^- \rightarrow e^-S^-$	$0.2549 \\ 103885.25$	0.1270 117914.80	6 4	$\frac{2}{2}$	4.372E-02 4.370E-02
	$287.24 \\ 0.00$	83801.95 84004.26	$\frac{4}{2}$	2 4	1.450E-01 2.916E-01		103860.74	117914.80	$\hat{2}$	$ar{2}$	4.377E-02
	0.00	83801.95	$\tilde{2}$	$\frac{4}{2}$	5.818E-01	$x^2P^o \rightarrow f^2S^e$	0.2549	0.0914	6	2	1.560E-02
$z^2P^o \rightarrow a^2D^e$	1.1997	0.6974	6	10	2.449E-03		$\begin{array}{c} 103885.25 \\ 103860.74 \end{array}$	$\frac{121814.38}{121814.38}$	4 2	$\frac{2}{2}$	1.560E-02 1.562E-02
	287.24	55325.18	4	6	2.201E-03	$x^2P^o \rightarrow g^2S^e$	0.2549	0.0690	6	2	7.671E-03
	$287.24 \\ 0.00$	55309.35 55309.35	4 2	4	2.444E-04 2.457E-03	w 1 , y 0	103885.25	124276.70	4	2	7.668E-03
$z^2P^o \rightarrow b^2D^e$	1.1997	0.4784	6	10	1.184E+00	0 0	103860.74	124276.70	2	2	7.678 E- 03
~ . , , , ,	287.24	79355.02	4	6	1.065E+00	$x^2P^o \rightarrow d^2D^e$	0.2549	0.1773	6	10	1.137E+00
	287.24	79338.50	4	4	1.183E-01		$\begin{array}{c} 103885.25 \\ 103885.25 \end{array}$	$\begin{array}{c} 112394.72 \\ 112394.56 \end{array}$	4 4	6 4	1.022E+00 1.136E-01
$z^2P^o \rightarrow c^2D^e$	0.00	79338.50	2	4	1.187E+00		103860.74	112394.56	2	4	1.139E+00
$z^{2}P^{3} \rightarrow c^{2}D^{3}$	$1.1997 \\ 287.24$	$0.2809 \\ 101024.35$	6 4	10 6	1.618E-01 1.455E-01	$x^2P^o o e^2D^e$	0.2549	0.1214	6	10	1.612E-01
	287.24	101023.05	4	4	1.617E-02		$\begin{array}{c} 103885.25 \\ 103885.25 \end{array}$	$\frac{118522.93}{118522.86}$	4	6 4	1.450E-01 1.611E-02
2	0.00	101023.05	2	4	1.621E-01		103860.74	118522.86	4 2	4	1.614E-01
$z^2 P^o o d^2 D^e$	1.1997	0.1773	6	10 6	4.073E-02 3.662E-02	$x^2P^o \rightarrow f^2D^e$	0.2549	0.0882	6	10	5.258E-02
	$287.24 \\ 287.24$	112394.72 112394.56	4 4	4	4.069E-03		103885.25	122163.54	4	6	4.730E-02
	0.00	112394.56	2	4	4.080E-02		$\begin{array}{c} 103885.25 \\ 103860.74 \end{array}$	$\frac{122163.48}{122163.48}$	$\frac{4}{2}$	4	5.256E-03 5.263E-02
$z^2 P^o o e^2 D^e$	1.1997	0.1214	6	10	1.593E-02	$x^2P^o \rightarrow g^2D^e$	0.2549	0.0670	6	10	2.378E-02
	$287.24 \\ 287.24$	$\begin{array}{c} 118522.93 \\ 118522.86 \end{array}$	4 4	6 4	1.433E-02 1.592E-03		103885.25	124495.70	4	6	2.140E-02
	0.00	118522.86	2	4	1.596E-02		$103885.25 \\ 103860.74$	124495.70	$\frac{4}{2}$	4 4	2.377E-03 2.380E-02
$z^2P^o o f^2D^e$	1.1997	0.0882	6	10	7.836E-03	$w^2P^o \rightarrow e^2S^e$	0.1629	$124495.70 \\ 0.1270$	6	2	4.157E-01
	287.24	122163.54	4	6	7.047E-03	w 1 -7 C D	113976.72	117914.80	4	2	4.152E-01
	$287.24 \\ 0.00$	$\begin{array}{c} 122163.48 \\ 122163.48 \end{array}$	$\frac{4}{2}$	4 4	7.830E-04 7.848E-03	00 -	113962.08	117914.80	2	2	4.168E-01
$z^2P^o \rightarrow g^2D^e$	1.1997	0.0670	6	10	4.426E-03	$w^2P^o o f^2S^e$	0.1629	0.0914	6	2	5.157E-02
	287.24	124495.70	4	6	3.980E-03		$\begin{array}{c} 113976.72 \\ 113962.08 \end{array}$	121814.38 121814.38	$\frac{4}{2}$	$\frac{2}{2}$	5.154E-02 5.163E-02
	287.24	124495.70	4	4	4.423E-04	$w^2 P^o \rightarrow g^2 S^e$	0.1629	0.0690	6	$\tilde{2}$	1.817E-02
$y^2P^o \rightarrow c^2S^e$	$0.00 \\ 0.4612$	124495.70 0.3087	$\frac{2}{6}$	4 2	4.433E-03 2.031E-01		113976.72	124276.70	4	2	1.816E-02
gı /es	81251.32	97972.09	4	$\tilde{2}$	2.028E-01	2 Do . 2 De	113962.08	124276.70	2	2	1.819E-02
0 0	81191.34	97972.09	2	2	2.036E-01	$w^2 P^o \to e^2 D^e$	$0.1629 \\ 113976.72$	0.1214 118522.93	6 4	10 6	1.291E+00 1.161E+00
$y^2P^o o d^2S^e$	0.4612	0.1883	6	2	4.160E-02		113976.72	118522.86	4	4	1.290E-01
	81251.32 81191.34	111184.46 111184.46	$\frac{4}{2}$	$\frac{2}{2}$	4.157E-02 4.165E-02	2.00	113962.08	118522.86	2	4	1.294E+00
$y^2P^o \rightarrow e^2S^e$	0.4612	0.1270	6	2	1.606E-02	$w^2P^o \rightarrow f^2D^e$	0.1629	0.0882	6 4	10 6	1.868E-01
•	81251.32	117914.80	4	2	1.605E-02		$\begin{array}{c} 113976.72 \\ 113976.72 \end{array}$	$\begin{array}{c} 122163.54 \\ 122163.48 \end{array}$	4	4	1.680E-01 1.867E-02
2 700 42 70	81191.34	117914.80	2	2	1.608E-02		113962.08	122163.48	$\bar{2}$	$ar{4}$	$1.870 ext{E-}01$
$y^2P^o o f^2S^e$	$0.4612 \\ 81251.32$	0.0914 121814.38	6 4	$\frac{2}{2}$	7.886E-03 7.883E-03	$w^2P^o o g^2D^e$	0.1629	0.0670	6	10	6.464E-02
	81191.34	121814.38	2	$\frac{2}{2}$	7.894E-03		$\begin{array}{c} 113976.72 \\ 113976.72 \end{array}$	$124495.70 \\ 124495.70$	4 4	6 4	5.814E-02 6.461E-03
$y^2P^o \rightarrow g^2S^e$	0.4612	0.0690	6	2	4.468E-03		113962.08	124495.70	2	4	6.470E-02
	81251.32	124276.70	4	2	4.466E-03	$v^2P^o \rightarrow f^2S^e$	0.1147	0.0914	6	2	2.360E-01
.2 Do2 De	81191.34	124276.70	2	2	4.472E-03	-	119273.81	121814.38	4	2	2.351E-01
$y^2P^o \rightarrow a^2P^e$	$0.4612 \\ 81251.32$	$0.4366 \\ 84004.26$	6 4	6 4	1.153E-05 9.779E-06	$v^2P^o \rightarrow g^2S^e$	119245.22	121814.38	2	2	2.378E-01
	81251.32	83801.95	4	2	1.812E-06	$\sigma I \rightarrow g^- S^-$	0.1147 119273.81	$0.0690 \\ 124276.70$	6 4	$\frac{2}{2}$	3.878E-02 3.871E-02
	81191.34	84004.26	2	4	3.997E-06		119245.22	124276.70	2	$\bar{2}$	3.893E-02
$y^2P^o \rightarrow c^2D^e$	81191.34	83801.95	2	2	7.419E-06	$v^2P^o o f^2D^e$	0.1147	0.0882	6	10	7.175E-01
$y^- F^- \rightarrow c^- D^0$	$0.4612 \\ 81251.32$	$0.2809 \\ 101024.35$	6 4	10 6	8.393E-01 7.546E-01		$\begin{array}{c} 119273.81 \\ 119273.81 \end{array}$	$\begin{array}{c} 122163.54 \\ 122163.48 \end{array}$	4 4	6 4	6.436E-01 7.151E-02
	81251.32	101023.05	4	4	8.384E-02		119245.22	122163.48	2	4	7.131E-02 7.222E-01
	81191.34	101023.05	2	4	8.409E-01						

TABLE II. Energies and Oscillator Strengths for Allowed Transitions in Si II See page 189 for Explanation of Tables

		•				_	Transition	E'.	F.			
Transition	$\frac{E_i}{\text{Ry/cm}^{-1}}$	$\frac{E_f}{\mathrm{Ry/cm^{-1}}}$	gi	<i>g</i> _f	fif		Transition	$\frac{E_i}{\mathrm{Ry/cm^{-1}}}$	$\frac{E_f}{\text{Ry/cm}^{-1}}$	gi	<i>g</i> _f	
$v^2P^o \rightarrow g^2D^e$	0.1147	0.0670	6	10	1.533E-01			103556.03	124948.40	8	8	7.998E-04
	119273.81	124495.70	4	6	1.377E-01		$z^2F^o \rightarrow e^2G^e$	$103556.16 \\ 0.2578$	$124948.40 \\ 0.0497$	6 14	8 18	2.879E-02 1.586E-02
	$\begin{array}{c} 119273.81 \\ 119245.22 \end{array}$	$124495.70 \\ 124495.70$	4 2	4 4	1.530E-02 1.539E-01		zr →eG	103556.03	126396.47	8	10	1.542E-02
$u^2P^o \rightarrow f^2S^e$	0.0939	0.0914	6	2	8.248E-02			103556.03	126396.47	8	8	4.406E-04
-	121590.19	121814.38	4	2	6.776E-02		$z^2F^o o f^2G^e$	$103556.16 \\ 0.2578$	$126396.47 \\ 0.0402$	$\frac{6}{14}$	8 18	1.586E-02 9.785E-03
$u^2P^o \rightarrow g^2S^e$	121444.12 0.0939	121814.38 0.0690	2 6	$\frac{2}{2}$	1.119E-01 3.924E-03		zr - j G	103556.03	127432.02	8	10	9.513E-03
$u \rightarrow g b$	121590.19	124276.70	4	2 2	3.854E-03			103556.03	127432.02	8	8 8	2.718E-04
270 4270	121444.12	124276.70	2		4.064E-03		$y^2F^o ightarrow e^2D^e$	103556.16 0.1648	$127432.02 \\ 0.1214$	6 14	10	9.784E-03 1.000E-01
$u^2P^o o f^2D^e$	0.0939 121590.19	$0.0882 \\ 122163.54$	$\frac{6}{4}$	10 6	3.965E-01 3.289E-01		g r ¬cD	113760.15	118522.93	8	6	1.000E-01
	121590.19	122163.48	4	4	3.654E-02			113760.32	118522.93	6	6	6.668E-03
200 200	121444.12	122163.48	2	4	4.585E-01		$y^2F^o \rightarrow f^2D^e$	$113760.32 \\ 0.1648$	$\begin{array}{c} 118522.86 \\ 0.0882 \end{array}$	$\frac{6}{14}$	4 10	9.335E-02 1.562E-02
$u^2P^o o g^2D^e$	0.0939 121590.19	$0.0670 \\ 124495.70$	$\frac{6}{4}$	10 6	6.697E-03 5.928E-03		g i , j D	113760.15	122163.54	8	6	1.562E-02
	121590.19	124495.70	4	4	6.587E-04			113760.32	122163.54	6	6	1.041E-03
2 2	121444.12	124495.70	2	4	6.918E-03		$y^2F^o o g^2D^e$	113760.32 0.1648	$122163.48 \\ 0.0670$	6 14	4 10	1.458E-02 5.552E-03
$t^2P^o \rightarrow g^2S^e$	0.0795	0.0690	6	$\frac{2}{2}$	6.756E-01		$g \vdash f \downarrow g \vdash D$	113760.15	124495.70	8	6	5.552E-03
	$\begin{array}{c} 123138.67 \\ 123097.63 \end{array}$	$\begin{array}{c} 124276.70 \\ 124276.70 \end{array}$	4 2	2	6.675E-01 6.916E-01			113760.32	124495.70	6	6	3.701E-04
$t^2P^o o g^2D^e$	0.0795	0.0670	6	10	1.802E+00		$y^2F^o \rightarrow a^2G^e$	$113760.32 \\ 0.1648$	$124495.70 \\ 0.1610$	6 14	4 18	5.181E-03 9.497E-02
	123138.67	124495.70	4	6	1.606E+00		y r - 7 u G	113760.15	114177.10	8	10	9.235E-02
	$\begin{array}{c} 123138.67 \\ 123097.63 \end{array}$	$124495.70 \\ 124495.70$	$\frac{4}{2}$	4 4	1.784E-01 1.838E+00			113760.15	114177.10	8	8	2.639E-03
$z^2D^o o d^2D^e$	0.2100	0.1773	10	10	7.467E-06		$y^2F^o o b^2G^e$	$113760.32 \\ 0.1648$	0.1118	6 14	8 18	9.495E-02 1.017E+00
	$\begin{array}{c} 108820.60 \\ 108820.60 \end{array}$	112394.72	6 6	6	6.937E-06		y r - y v G	113760.15	119578.23	8	10	9.883E-01
	108778.70	$\begin{array}{c} 112394.56 \\ 112394.72 \end{array}$	4	4 6	4.955E-07 7.520E-07			113760.15	119578.23	8	8	2.824E-02
	108778.70	112394.56	4	4	6.767 E-06		$y^2F^o o c^2G^e$	113760.32 0.1648	$119578.23 \\ 0.0821$	$\frac{6}{14}$	8 18	1.017E+00 2.274E-01
$z^2D^o o e^2D^e$	0.2100	0.1214	10	10	2.382E-05		y r -> t G	113760.15	122835.13	8	10	2.211E-01
	$\begin{array}{c} 108820.60 \\ 108820.60 \end{array}$	$\begin{array}{c} 118522.93 \\ 118522.86 \end{array}$	6 6	6 4	2.220E-05 1.585E-06			113760.15	122835.13	8	8	6.317E-03
	108778.70	118522.93	4	6	2.388E-06		$y^2F^o \rightarrow d^2G^e$	$113760.32 \\ 0.1648$	$122835.13 \\ 0.0629$	$\frac{6}{14}$	8 18	2.274E-01 8.942E-02
2 D0 . t2 De	108778.70	118522.86	4	4	2.150E-05		y r - , u G	113760.15	124948.40	8	10	8.694E-02
$z^2D^o o f^2D^e$	$0.2100 \\ 108820.60$	$0.0882 \\ 122163.54$	10 6	10 6	3.456E-05 3.222E-05			113760.15	124948.40	8	8	2.484E-03
	108820.60	122163.48	6	4	2.301E-06		$y^2F^o \rightarrow e^2G^e$	$113760.32 \\ 0.1648$	$124948.40 \\ 0.0497$	6 14	8 18	8.942E-02 4.527E-02
	108778.70	122163.54	4	6	3.463E-06		y r → e G	113760.15	126396.47	8	10	4.402E-02
$z^2D^o o g^2D^e$	$108778.70 \\ 0.2100$	$\begin{array}{c} 122163.48 \\ 0.0670 \end{array}$	4 10	4 10	3.117E-05 4.043E-05			113760.15	126396.47	8	8	1.258E-03
~ D , g D	108820.60	124495.70	6	6	3.769E-05		$y^2F^o \rightarrow f^2G^e$	113760.32 0.1648	$126396.47 \\ 0.0402$	$\frac{6}{14}$	8 18	4.527E-02 2.659E-02
	$\begin{array}{c} 108820.60 \\ 108778.70 \end{array}$	124495.70	6	4 6	2.692E-06		y r j G	113760.15	127432.02	8	10	2.585E-02
	108778.70	$124495.70 \\ 124495.70$	4 4	4	4.050E-06 3.645E-05			113760.15	127432.02	8	8	7.386E-04
$z^2F^o o d^2D^e$	0.2578	0.1773	14	10	4.262E-02		$x^2F^o \rightarrow f^2D^e$	$113760.32 \\ 0.1142$	$127432.02 \\ 0.0882$	6 14	8 10	2.659E-02 1.658E-01
	103556.03	112394.72	8 6	6 6	4.262E-02		$x \mapsto f D$	119311.19	122163.54	8	6	1.658E-01
	103556.16 103556.16	$\begin{array}{c} 112394.72 \\ 112394.56 \end{array}$	6	4	2.841E-03 3.978E-02			119311.34	122163.54	6	6	1.105 E-02
$z^2 F^o ightarrow e^2 D^e$	0.2578	0.1214	14	10	6.594E-03		$x^2F^o \rightarrow g^2D^e$	$119311.34 \\ 0.1142$	$122163.48 \\ 0.0670$	6 14	4 10	1.548E-01 2.647E-02
	103556.03 103556.16	118522.93	8	6	6.594E-03		$x \vdash \neg y \vdash D$	119311.19	124495.70	8	6	2.647E-02 2.647E-02
	103556.16	$\begin{array}{c} 118522.93 \\ 118522.86 \end{array}$	6 6	6 4	4.396E-04 6.155E-03			119311.34	124495.70	6	6	1.765E-03
$z^2F^o o f^2D^e$	0.2578	0.0882	14	10	2.304E-03		$x^2F^o \rightarrow b^2G^e$	$119311.34 \\ 0.1142$	$\begin{array}{c} 124495.70 \\ 0.1118 \end{array}$	6 14	4 18	2.470E-02 1.919E-01
	103556.03	122163.54	8 6	6	2.304E-03		w1 /00	119311.19	119578.23	8	10	1.866E-01
	103556.16 103556.16	$\begin{array}{c} 122163.54 \\ 122163.48 \end{array}$	6	6 4	1.536E-04 2.150E-03			119311.19	119578.23	8	8	5.331E-03
$z^2F^o o g^2D^e$	0.2578	0.0670	14	10	1.107E-03		$x^2F^o \rightarrow c^2G^e$	119311.34 0.1142	119578.23 0.0821	6 14	8 18	1.918E-01 8.789E-01
	103556.03 103556.16	124495.70	8	6	1.107E-03		# 1 -7 C G	119311.19	122835.13	8	10	8.545E-01
	103556.16	$124495.70 \\ 124495.70$	6 6	6 4	7.377E-05 1.033E-03			119311.19	122835.13	8		2.441E-02
$z^2F^o ightarrow a^2G^e$	0.2578	0.1610	14	18	1.234E+00		$x^2F^o \rightarrow d^2G^e$	$119311.34 \\ 0.1142$	122835.13 0.0629	6 14	8 18	8.789E-01 2.303E-01
	103556.03	114177.10	8	10	1.200E+00		x r -7 a G	119311.19	124948.40	8	10	2.239E-01
	103556.03 103556.16	$114177.10 \\ 114177.10$	8 6	8 8	3.428E-02 1.234E+00			119311.19	124948.40	8	8	6.398E-03
$z^2F^o ightarrow b^2G^e$	0.2578	0.1118	14	18	1.893E-01		$x^2F^o \rightarrow e^2G^e$	119311.34 0.1142	124948.40 0.0497	6	8 18	2.303E-01 9.796E-02
	103556.03	119578.23	8	10	1.840E-01		ω 1 -7 c G	119311.19	126396.47	14 8	10	9.796E-02 9.524E-02
	103556.03 103556.16	$\begin{array}{c} 119578.23 \\ 119578.23 \end{array}$	8 6	8 8	5.258E-03 1.893E-01			119311.19	126396.47	8	8	2.721E-03
$z^2 F^o o c^2 G^e$	0.2578	0.0821	14	18	6.249E-02		$x^2F^o \rightarrow f^2G^e$	$119311.34 \\ 0.1142$	126396.47	6	8 18	9.795E-02 5.200E-02
	103556.03	122835.13	8	10	6.076E-02		$x \mapsto f^-G^-$	119311.19	$0.0402 \\ 127432.02$	14 8	10	5.056E-02
	103556.03 103556.16	$\begin{array}{c} 122835.13 \\ 122835.13 \end{array}$	8 6	8 8	1.736E-03 6.249E-02			119311.19	127432.02	8	8	1.444 <u>E</u> -03
$z^2 F^o o d^2 G^e$	0.2578	0.0629	14	18	2.879E-02		$w^2F^o \rightarrow g^2D^e$	119311.34 0.0838	127432.02 0.0670	6 14	8	5.200E-02 2.374E-01
	103556.03	124948.40	8	10	2.799E-02		$\omega \vdash \neg g D$	0.0038	0.0070	14	10	4.514E-UI

TABLE II. Energies and Oscillator Strengths for Allowed Transitions in Si II See page 189 for Explanation of Tables

ransition	$\frac{E_i}{\mathrm{Ry/cm^{-1}}}$	E_f Ry/cm ⁻¹	g_i	g_f	f_{if}	Transition	$\frac{E_i}{\mathrm{Ry/cm^{-1}}}$	E_f Ry/cm ⁻¹	g_i	g_f	f_{if}
· · · · · · · · · · · · · · · · · · ·			0		2.375E-01	12 00 2 00					0.0505.
	$\substack{122655.25 \\ 122655.37}$	$124495.70 \\ 124495.70$	8 6	6 6	1.583E-01	$h^2S^e o q^2P^o$	0.0537	0.0481	2	6	3.270E+
	122655.37	124495.70	6	4	2.216E-01		*		2	4 2	2.180E+
$v^2F^o \rightarrow c^2G^e$	0.0838	0.0821	14	18	2.912E-01	$h^2D^e \rightarrow g^2P^o$	0.0534	0.0491	$\frac{2}{10}$	6	1.090E+ 9.680E-0
	122655.25	122835.13	8	10	2.832E-01	$h^-D^- \to q^-P^-$	0.0524	0.0481	6	4	9.680E-0
	$\begin{array}{c} 122655.25 \\ 122655.37 \end{array}$	122835.13	8	8	8.090E-03		*		4	4	1.613E-0
2 170 12 00		122835.13	6	8	2.911E-01		*		4	2	8.067E-0
$v^2 F^o o d^2 G^e$	0.0838	0.0629	14	18	8.037E-01	$h^2D^e \rightarrow u^2F^e$	0.0524	0.0504	10	14	1.240E+
	$\substack{122655.25 \\ 122655.25}$	124948.40 124948.40	8 8	10 8	7.814E-01 2.233E-02	,,,,,,	*		6	8	1.181E+
	122655.37	124948.40	6	8	8.037E-01		*		6	6	5.905E-0
$v^2F^o \rightarrow e^2G^e$	0.0838	0.0497	14	18	2.256E-01		*		4	6	1.240E+
,,,,	122655.25	126396.47	8	10	2.193E-01	$h^2D^e \rightarrow t^2F^o$	0.0524	0.0408	10	14	2.390E-0
	122655.25	126396.47	8	8	6.267E-03		*	•	6	8	$2.276\mathrm{E}$
0	122655.37	126396.47	6	8	2.256E-01		**		6	6	1.138E-
$v^2F^o o f^2G^e$	0.0838	0.0402	14	18	1.001E-01	12 Da 2 Ta			4	6	2.390E-
	122655.25	$\begin{array}{c} 127432.02 \\ 127432.02 \end{array}$	8 8	10 8	9.729E-02 2.780E-03	$i^2D^e o t^2F^o$	0.0422	0.0408	10	14	1.410E+
	$\begin{array}{c} 122655.25 \\ 122655.37 \end{array}$	127432.02	6	8	1.001E-01		*		6	8	1.343E-
$^2F^o \rightarrow d^2G^e$	0.0640	0.0629	14	18	3.953E-01		*	ı	6 4	6 6	6.714E-0 1.410E-
1 / 4 G	124822.08	124948.40	8	10	3.844E-01	$a^2G^e \rightarrow z^2H^c$	0.1608	0.1112	18	22	1.650E
	124822.08	124948.40	8	8	1.098E-02	4 G -7 Z H	0.1006 *	0.1112	10	12	1.620E-
	124822.14	124948.40	6	8	3.952E-01		*	•	10	10	3.000E-
$e^2F^o \rightarrow e^2G^e$	0.0640	0.0497	14	18	7.524E-01		*	•	8	10	1.650E
	124822.08	126396.47	8	10	7.316E-01	$a^2G^e \rightarrow y^2H^c$	0.1608	0.0817	18	22	2.061E-
	$\begin{array}{c} 124822.08 \\ 124822.14 \end{array}$	$\begin{array}{c} 126396.47 \\ 126396.47 \end{array}$	8 6	8 8	2.090E-02 7.524E-01	a a , y 11	*	, 0.0011	10	12	2.024E-
$^2F^o \rightarrow f^2G^e$	0.0640	0.0402	14	18	2.198E-01		*	•	10	10	3.747E-
r -7	124822.08	127432.02	8	10	2.137E-01		*	•	8	10	2.061E-
	124822.08	127432.02	8	8	6.107E-03	$a^2G^e \rightarrow x^2H^c$	0.1608	0.0626	18	22	6.167E-
	124822.14	127432.02	6	8	2.198E-01		*	•	10	12	6.055E-
$^2F^o ightarrow e^2G^e$	0.0505	0.0497	14	18	4.892E-01		*		10	10	1.121E-
	126304.82	126396.47	8	10	4.756E-01	0		•	8	10	6.167E-
	126304.82	126396.47	8 6	8	1.359E-02	$a^2G^e o w^2H$	0.1608	0.0494	18	22	2.683E-
$a^2F^o \to f^2G^e$	126304.82	126396.47		8	4.892E-01		1		10	12	2.635E-
$i^*F^* \rightarrow j^*G^*$	$0.0505 \\ 126304.82$	$0.0402 \\ 127432.02$	14 8	18 10	7.195E-01 6.995E-01			· t	10 8	10 10	4.879E-
	126304.82	127432.02	8	8	1.998E-02	$a^2G^e \rightarrow v^2H^c$	0.1000	0.0400	18	22	2.683E- 1.422E-
	126304.82	127432.02	6	8	7.195E-01	$a^-G^- \rightarrow v^-H^-$	0.1608	0.0400	10	12	1.422E- 1.396E-
$^2F^o \rightarrow f^2G^e$	0.0408	0.0402	14	18	4.970E-01		×	k	10	10	2.586E-
-	127363.50	127432.02	8 8	10	4.832E-01		*	k	8	10	1.422E-
	127363.50	127432.02	8	8	1.380E-02	$b^2G^e \rightarrow z^2H^c$	0.1117	0.1112	18	22	2.106E-
$z^4P^e \rightarrow z^4S^o$	127363.50	127432.02	6	8	4.970E-01		*	k	10	12	2.067E-
$z \cdot P \cdot \rightarrow z \cdot S \cdot$	$0.8096 \\ 43107.91$	$0.0803 \\ 123033.50$	$^{12}_{6}$	4 4	2.893E-01 2.889E-01		*	k	10	10	3.828E-
	42932.62	123033.50	4	4	2.895E-01		,	k	8	10	2.106E-
	42824.29	123033.50	$\hat{2}$	$\tilde{4}$	2.899E-01	$b^2G^e \rightarrow y^2H^e$	0.1117	0.0817	18	22	1.450E-
$z^4P^e \rightarrow z^4P^o$	0.8096	0.1348	12	12	3.364E-01		*	k	10	12	1.424E-
	43107.91	117178.06	6	6	2.355E-01		,	K	10	10	2.636E-
	43107.91	116978.38	6	4	1.007E-01	.0 0			8	10	1.450E
	42932.62	117178.06	4	6	1.518E-01	$b^2G^e \to x^2H^c$	0.1117	0.0626	18	22	2.683E
	$\begin{array}{c} 42932.62 \\ 42932.62 \end{array}$	$\begin{array}{c} 116978.38 \\ 116862.38 \end{array}$	4 4	$\frac{4}{2}$	4.485E-02 1.399E-01		,	r	10	12	2.635E-
	42824.29	116978.38	2	4	2.807E-01		,	k	10 8	10 10	4.879E- 2.683E-
	42824.29	116862.38	$\frac{2}{2}$	$\tilde{2}$	5.605E-02	$b^2G^e \rightarrow w^2H$	0.1117	0.0404		22	9.500E-
$^4P^e \rightarrow y^4P^o$	0.8096	0.0661	12	12	3.240E-01	$0^-G^- \rightarrow w^-H$	0.1117	0.0494 *	18 10	12	9.327E
·	43107.91	124567.40	6	6	2.264E-01		,	k	10	10	1.727E-
	43107.91	124615.60	6	4	9.711E-02		,	k	8	10	9.500E
	42932.62	124567.40	4	6	1.459E-01	$b^2G^e \rightarrow v^2H^c$	0.1117	0.0400	18	22	4.539E
	42932.62 42932.62	$\begin{array}{c} 124615.60 \\ 124638.90 \end{array}$	4 4	$\frac{4}{2}$	4.325E-02 1.352E-01	0 4 7 0 11	, , , , , , , , , , , , , , , , , , ,	*	10	12	4.456E
	42824.29	124615.60	2	$\frac{2}{4}$	2.707E-01		,	k	10	10	8.253E
	42824.29	124638.90	$\bar{2}$	$\bar{2}$	5.415E-02		,	*	8	10	4.539E
$^4P^e \rightarrow z^4D^o$	0.8096	0.0681	12	20	1.255E+00	$c^2G^e \rightarrow y^2H^c$	0.0820	0.0817	18	22	3.989E
	43107.91	124449.50	6	8	1.004E+00	v	,	k	10	12	3.916E
	43107.91	124316.90	6	6	2.255E-01		3		10	10	7.253E
	43107.91	124325.30	6	4	2.506E-02		•		8	10	3.989E
	$\begin{array}{c} 42932.62 \\ 42932.62 \end{array}$	$\begin{array}{c} 124316.90 \\ 124325.30 \end{array}$	4	6 4	7.909E-01 4.018E-01	$c^2G^e \rightarrow x^2H^e$	0.0820	0.0626	18	22	1.339E
	42932.62	124325.30	4	2	6.279E-02		;	*	10	12	1.315E
	42824.29	124325.30	2	$\frac{2}{4}$	6.286E-01		•	*	10	10	2.434E
	42824.29	124337.30	$\overline{2}$	$\overline{2}$	6.287E-01	0 0		·	8	10	1.339E
			2	6	3.185E-01	$c^2G^e \rightarrow w^2H$	0.0820	0.0494	18	22	$2.906\mathrm{E}$
$^2S^e \rightarrow r^2P^o$	0.0537	0.0525	4								0 0-0-
$r^2 S^e \rightarrow r^2 P^o$		* *	2 2	4 2	2.123E-01 1.062E-01			*	10 10	12 10	2.853E- 5.283E-

TABLE II. Energies and Oscillator Strengths for Allowed Transitions in Si II See page 189 for Explanation of Tables

Transition	E_{i}	E_f	g_i	<i>g</i> _{f}	f_{if}	Transit	ion	E_i	E_f	gi	g_f	f_{if}
	Ry/cm ⁻¹	Ry/cm ⁻¹						Ry/cm ⁻¹	Ry/cm ⁻¹			
$c^2G^e \rightarrow v^2H^o$	0.0820	0.0400	18	22	1.122E-01	2 70	2 110	*		12	14	3.254E-01
	*		10 10	12 10	1.102E-01 2.040E-03	$c^2 I^e \rightarrow$	· v ² H ·	0.0494	0.0400	$\frac{26}{14}$	22	2.969E-02 2.969E-02
	*	:	8	10	1.122E-01			*	•	12	$\frac{12}{12}$	2.969E-02 4.499E-04
$d^2G^e \rightarrow x^2H^o$	0.0628	0.0626	18	22	5.667E-02			*	•	12	10	2.924E-02
	*	·	10	12	5.564E-02	$c^2 I^e \rightarrow$	y^2K^o	0.0494	0.0494	26	30	1.261E-03
	*		10	10	1.030E-03			*		14	16	1.249E-03
$d^2G^e \rightarrow w^2H^o$	0.0628	0.0494	8 18	$\frac{10}{22}$	5.667E-02 1.272E+00			7		14	14	1.201E-05
$u G \rightarrow w H$	U.UU20 *	0.0494	10	12	1.249E+00	$c^2 I^e \rightarrow$	$r^2 K^o$	0.0494	0.0400	$\frac{12}{26}$	14 30	1.262E-03 1.985E+00
	*	t .	10	10	2.313E-02	C 1 /	<i>w</i> 11	*	0.0400	14	16	1.966E+00
	*	•	8	10	1.272E+00			×	•	14	14	1.890E-02
$d^2G^e \rightarrow v^2H^o$	0.0628	0.0400	18	22	3.000E-01	20 = 2	2	*	•	12	14	1.985E+00
	*	•	10 10	12 10	2.945E-01 5.455E-03	$d^2I^e \rightarrow$	x^2K^0	0.0400	0.0400	26	30	2.242E-03
	*	•	8	10	3.000E-01			*		14 14	16 14	2.221E-03 2.136E-05
$e^2G^e \rightarrow w^2H^o$	0.0496	0.0494	18	22	7.278E-02			×	•	12	14	2.242E-03
	*	•	10	12	7.145E-02	a^2L^e -	$+ x^2 K^o$	0.0494	0.0400	34	30	4.353E-03
	*	•	10	10	1.323E-03			*		18	16	4.353E-03
$e^2G^e \rightarrow v^2H^o$	0.0496	0.0400	8 18	10 22	7.278E-02 1.239E+00					16	16	3.627E-05
e G -70 II	**	0.0400	10	12	1.235E+00 1.216E+00	27 e	$\rightarrow z^2 M^o$	0.0494	0.0400	16 34	14 38	4.317E-03 3.000E+00
	*	•	10	10	2.253E-02	u D -	7 & IVI	V.0454	0.0400	18	20	2.982E+00
.0 - 0	*	•	8	10	1.239E+00			*	¢	18	18	1.754E-02
$f^2G^e \rightarrow v^2H^o$	0.0401	0.0400	18	22	8.722E-02	-0	0	*	•	16	18	3.000E+00
	*	•	10 10	12 10	8.564E-02 1.586E-03	b^2L^e —	$\rightarrow z^2 M^o$	0.0400	0.0400	34	38	6.147E-07
	*	•	8	10	8.722E-02			- k		18 18	$\frac{20}{18}$	6.111E-07 3.595E-09
$a^2I^e ightarrow x^2H^o$	0.0816	0.0626	26	22	5.769E-03			×	•	16	18	6.147E-07
	*		14	12	5.769E-03	$z^2 P^o$ –	$\rightarrow h^2 S^e$	1.2014	0.0537	6	2	6.867E-04
	*	`	$\frac{12}{12}$	12 10	8.741E-05 5.682E-03			*	•	4	2	6.867E-04
$a^2I^e \rightarrow w^2H^o$	0.0816	0.0494	26	22	7.539E-04	z² Pº -	·2 cre	* * * * * * * * * * * * * * * * * * * *		2	2	6.867E-04
	*	*	14	12	7.539E-04	2º Pº -	→ 1°5°	1.2014	0.0431	6 4	$\frac{2}{2}$	4.850E-04 4.850E-04
	k 	k	12	12	1.142E-05			*	k	2	2	4.850E-04
2 Te . 2 TTO	0.0014	0.0400	12	10	7.424E-04	z^2P^o –	$\rightarrow b^2 P^e$	1.2014	0.0064	$\bar{6}$	6	2.417E-03
$a^2I^e \rightarrow v^2H^o$	0.0816	0.0400	$\frac{26}{14}$	$\frac{22}{12}$	2.173E-04 2.173E-04			×	k 	4	4	2.014E-03
	×	k	12	12	3.293E-06			,	r k	4 2	2	4.028E-04
	×	k	12	10	2.140E-04			a	k	$\frac{2}{2}$	$\frac{4}{2}$	8.056E-04 1.611E-03
$a^2I^e \rightarrow z^2K^o$	0.0816	0.0625	26	30	2.338E+00	$z^2 P^{\circ}$ –	$\rightarrow h^2 D^e$	1.2014	0.0524	6	10	2.750E-03
	,	r k	14 14	16 14	2.316E+00 2.227E-02			×	k	4	6	2.475E-03
	*	k	12	14	2.339E+00			,	*	4	4	2.750E-04
$a^2I^e \rightarrow y^2K^o$	0.0816	0.0494	26	30	2.289E-01	~2 Do	$\rightarrow i^2 D^e$	1.2014	0.0422	2 6	4 10	2.750E-03 1.817E-03
	,	k	14	16	2.267E-01	z	7 1 D	1.2014	V.U422	4	6	1.635E-03
	*	k k	14	14	2.180E-03			*	k	$\hat{4}$	4	1.817E-04
$a^2I^e \rightarrow x^2K^o$	0.0816	0.0400	12 26	14 30	2.289E-01 5.885E-02		_	*	k	2	4	1.817E-03
u i ¬ x ii	*	k 0.0400	14	16	5.829E-02	y^2P^o –	$\rightarrow h^2 S^e$	0.4637	0.0537	6	2	2.817E-03
	*	k	14	14	5.604E-04			- *	k	$\frac{4}{2}$	$\frac{2}{2}$	2.817E-03 2.817E-03
.2	*	k	12	14	5.885E-02	y^2P^o –	$\rightarrow i^2 S^e$	0.4637	0.0431	6	2	1.883E-03
$b^2 I^e \to w^2 H^o$	0.0625	0.0494	26	$\frac{22}{12}$	1.600E-02 1.600E-02	9 1	, , ,	0.1001	k 0.0401	4	2	1.883E-03
	*	k	14 12	12	2.424E-04		_	3	k	2	2	1.883E-03
	*	k	12	10	1.576E-02	y^2P^o -	$\rightarrow b^2 P^e$	0.4637	0.0064	6	6	1.348E-02
$b^2 I^e \rightarrow v^2 H^o$	0.0625	0.0400	26	22	2.346E-03			,	* k	4	4	1.124E-02 2.247E-03
	*	k	14	12	2.346E-03			*	k	$\frac{4}{2}$	$\frac{2}{4}$	4.494E-03
	,	r k	12	12	3.555E-05			*	k	$\frac{7}{2}$	2	8.989E-03
$b^2 I^e \rightarrow z^2 K^o$	0.0625	0.0625	$\frac{12}{26}$	10 30	2.311E-03 4.654E-04	$y^2 P^o$ -	$\rightarrow h^2 D^e$	0.4637	0.0524	6	10	4.833E-03
01 -72 K	0.0023	*	14	16	4.609E-04			,	k L	4	6	4.350E-03
	,	*	14	14	4.432E-06			,	r k	4	4	4.833E-04
12 70 2		*	12	14	4.654E-04	,,2 po_	$\rightarrow i^2 D^e$	0.4637	0.0422	2 6	4 10	4.833E-03 2.933E-03
$b^2 I^e \to y^2 K^o$	0.0625	0.0494 *	26	30	2.123E+00 2.103E+00	<i>y</i> 1	,,,,	0.4037	v.U442 k	4	6	2.640E-03
		*	14 14	16 14	2.103E+00 2.022E-02			,	k	4	4	2.933E-04
	,	*	12	14	2.123E+00	2	12 ~~			2	4	2.933E-03
$b^2I^e \rightarrow x^2K^o$	0.0625	0.0400	26	30	3.254E-01	x^2P^o -	$\rightarrow h^2 S^e$	0.2564	0.0537	6	2	4.467E-03
		*	14	16	3.223E-01			,	k	$\frac{4}{2}$	$\frac{2}{2}$	4.467E-03 4.467E-03
	·		14	14	3.099E-03	x^2P^o -	$\rightarrow i^2 S^e$	0.2564	0.0431	6	2	2.850E-03
								5.2001	3.0101		-	2.00011 00

TABLE II. Energies and Oscillator Strengths for Allowed Transitions in Si II See page 189 for Explanation of Tables

ransition	$\frac{E_i}{\mathrm{Ry/cm^{-1}}}$	$\frac{E_f}{\text{Ry/cm}^{-1}}$	g_i	g_f	f_{if}		Transition	E_i Ry/cm ⁻¹	$\frac{E_f}{\mathrm{Ry/cm^{-1}}}$	g_i	g_f	
	*		4	2	2.850E-03			*	:	2	4	1.3
	*		2	2	2.850E-03	t	$^2P^o \rightarrow h^2S^e$	0.0802	0.0537	6	2	6.4
$^{o} \rightarrow b^{2}P^{e}$	0.2564	0.0064	6	6	7.917E-03			*		4	2	6.4
	*		4	4	6.597 E-03		$^{2}P^{o} \rightarrow i^{2}S^{e}$	0.0000	0.0421	2	2	6.4
	*		4	2	1.319E-03	τ	$r^2P^3 \rightarrow r^2S^3$	0.0802	0.0431	6 4	$\frac{2}{2}$	$\frac{2.0}{2.0}$
	*		2 2	4 2	2.639E-03 5.278E-03			*	:	2	2	2.0
$P^o o h^2 D^e$	0.2564	0.0524	6	10	1.305E-02	t	$^{2}P^{o} \rightarrow b^{2}P^{e}$	0.0802	0.0064	6	6	9.6
$I \rightarrow h D$	0.2304 *	0.0324	4	6	1.175E-02			*		4	4	8.0
	*		$\hat{4}$	4	1.305E-03			*		4	2	1.6
	*		2	4	1.305E-02			7		2	4	3.2
$P^o \rightarrow i^2 D^e$	0.2564	0.0422	6	10	7.933E-03		$^{2}P^{o} \rightarrow h^{2}D^{e}$	0.0802	0.0524	$\frac{2}{6}$	2 10	6.4 1.8
	*		4	6	7.140E-03 7.933E-04	,	$\Gamma \rightarrow n D$	0.0002	0.0324	4	6	1.6
	*		$\frac{4}{2}$	4	7.933E-04 7.933E-03			*	ı	$\hat{4}$	4	1.8
$P^o \rightarrow h^2 S^e$	0.1625	0.0537	6	2	8.900E-03			*	•	2	4	1.8
. , ,, ,	**	0.000.	4	$\bar{2}$	8.900E-03	t	$i^2P^o \rightarrow i^2D^e$	0.0802	0.0422	6	10	5.6
	*		2	2	8.900E-03			**	:	4	6	5.0
$P^o o i^2 S^e$	0.1625	0.0431	6	2	5.167E-03			*	•	4	4 4	5.6 5.6
	*		4	2	5.167E-03	,	$s^2 P^o \rightarrow h^2 S^e$	0.0622	0.0537	6	2	8.0
Do , 12 De	0.100*	0.0064	2	2	5.167E-03	•		× 2.00.2		4	2	8.0
$^{2}P^{o} \rightarrow b^{2}P^{e}$	0.1625	0.0064	6 4	6 4	1.578E-02 1.315E-02			*	•	2	2	8.0
	*		4	2	2.631E-03		$s^2 P^o \rightarrow i^2 S^e$	0.0622	0.0431	6	2	8.0
	*		2	4	5.261E-03			×	•	4	2	8.0
	*		2	2	1.052E-02		$b^2 P^o \rightarrow b^2 P^e$	0.0000	0.0004	2	$\frac{2}{6}$	8.0
$P^o \rightarrow h^2 D^e$	0.1625	0.0524	6	10	3.100E-02	ě	s-P- → 0-P-	0.0622	0.0064	6 4	4	4.4 3.6
	*		4	6	2.790E-02			*	•	4	2	7.3
	*		$\frac{4}{2}$	4 4	3.100E-03 3.100E-02			*	•	$\dot{2}$	4	1.4
$P^o \rightarrow i^2 D^e$	0.1625	0.0422	6	10	1.767E-02			*	•	2	2	$^{2.9}$
	0.1025 *	0.0422	4	6	1.590E-02		$s^2 P^o \to h^2 D^e$	0.0622	0.0524	6	10	2.0
	*		4	4	1.767E-03					4	6	$\frac{1.8}{2.0}$
	*		2	4	$1.767 ext{E-}02$,	•	$\frac{4}{2}$	4 4	2.0
$P^o o h^2 S^e$	0.1166	0.0537	6	2	1.505E-02		$s^2 P^o \rightarrow i^2 D^e$	0.0622	0.0422	6	10	2.3
	77 24		4	$\frac{2}{2}$	1.505E-02	•	,,,,,	0.0022	. 0.0122	4	6	2.1
$P^o ightarrow i^2 S^e$	0.1166	0.0431	2 6	2	1.505E-02 7.567E-03			*	•	4	4	2.3
1 715	V.1100 *	0.0431	4	$\tilde{2}$	7.567E-03		2 200 12 00	,		2	4	2.3
	*	ŧ	2	2	7.567E-03	1	$r^2P^o \rightarrow i^2S^e$	0.0525	0.0431	6	$\frac{2}{2}$	8.2 8.2
$P^o ightarrow b^2 P^e$	0.1166	0.0064	6	6	9.867 E-02			•	•	4 2	$\frac{2}{2}$	8.2
	*	:	4	4	$8.222 ext{E-}02$	1	$r^2P^o \rightarrow b^2P^e$	0.0525	0.0064	6	6	9.9
	7	,	4	2	1.644E-02			,	•	4	4	8.3
		,	$\frac{2}{2}$	4 2	3.289E-02 6.578E-02					4	2	1.6
$P^o \rightarrow h^2 D^e$	0.1166	0.0524	6	10	6.600E-02			,		2	4	3.3
$I \rightarrow n D$	V.1100 *	0.0024	4	6	5.940E-02		$r^2P^o \to h^2D^e$	0.0505	0.0504	2	2	6.6
	*	•	$\hat{4}$	4	6.600E-03	1	$r \to n^- D^\circ$	0.0525	0.0524	6 4	10 6	$\frac{1.3}{1.1}$
			2	4	6.600E-02			*	•	4	4	1.3
$P^o o i^2 D^e$	0.1166	0.0422	6	10	3.567E-02		_	*	•	2	$\overline{4}$	1.3
	**************************************	- t	4	6 4	3.210E-02 3.567E-03	1	$r^2P^o \rightarrow i^2D^e$	0.0525	0.0422	6	10	1.9
	*	•	4 2	4	3.567E-03 3.567E-02				s k	4	6	1.7
$P^o \rightarrow h^2 S^e$	0.1011	0.0537	6	2	1.225E-03			,	•	4	4	1.9
- /10 D	3.1011	. 0.0001	4	$\frac{2}{2}$	1.225E-03		$q^2P^o \rightarrow i^2S^e$	0.0481	0.0431	$\frac{2}{6}$	4 2	$\frac{1.9}{9.2}$
	k	•	2	$\overline{2}$	1.225E-03	•	4 1 7 1 3	0.0401	v.0431	4	2	9.2
$^{i}P^{o} \rightarrow i^{2}S^{e}$	0.1011	0.0431	6	2	5.300 E-04			,	*	2.	2	9.2
	:		4	2	5.300E-04		$q^2P^o \rightarrow b^2P^e$	0.0481	0.0064	6	6	5.6
D0 . 12 D4	0.1011	0.000:	2	2	5.300E-04			•	k	4	4	4.6
$P^o o b^2 P^e$	0.1011	0.0064	6	6	1.483E-01				k v	4	2	9.3
		•	4 4	$\frac{4}{2}$	1.236E-01 2.472E-02			,	r k	2	$\frac{4}{2}$	1.8
	,	k	2	4	4.944E-02		$g^2P^o \rightarrow i^2D^e$	0.0481	0.0422	2 6	10	$\frac{3.7}{2.2}$
	,	*	$\tilde{2}$	2	9.889E-02	'	y i ¬iD	0.0401	v.0422	4	6	2.0
$P^o o h^2 D^e$	0.1011	0.0524	6	10	1.242E-04			•	k	4	4	2.2
		k	4	6	1.118E-04		0	3	×	2	4	2.2
	,	r k	4	4	1.242E-05		$z^2D^o o b^2P^e$	0.2302	0.0064	10	6	9.0
$^{2}P^{o} \rightarrow i^{2}D^{e}$	0.1011	0.0400	2	10	1.242E-04			,	k k	6	4	9.0
$i \rightarrow i D^{\circ}$	0.1011	0.0422	6 4	10 6	1.307E-04 1.176E-04			,	k	4 4	4 2	1.5 7.5
			-1	U	1.307E-05					4	4	6.1

TABLE II. Energies and Oscillator Strengths for Allowed Transitions in Si II See page 189 for Explanation of Tables

ransition	E_i Ry/cm ⁻¹	$\frac{E_f}{\mathrm{Ry/cm^{-1}}}$	g_i	<i>g</i> _f	f_{if}
$o \rightarrow h^2 D^e$	0.2302	0.0524	10	10	4.830E-05
	*		6 6	6 4	4.508E-05 3.220E-06
	*		4	6	4.830E-06
	*		4	4	4.347E-05
$D^o o i^2 D^e$	0.2302	0.0422	10	10	4.790E-05
	*		6 6	6 4	4.471E-05 3.193E-06
	*		4	6	4.790E-06
	*		4	4	4.311E-05
$F^o o h^2 D^e$	0.2576	0.0524	14 8	10 6	6.271E-04 6.271E-04
	*		6	6	4.181E-05
	*		6	4	5.853E-04
$F^o o i^2 D^e$	0.2576	0.0422	14 8	10 6	3.957E-04 3.957E-04
	*		6	6	2.638E-05
_	*		6	4	3.693E-04
$f^o o h^2 D^e$	0.1646	0.0524	14	10	2.707E-03
	*		8 6	6 6	2.707E-03 1.805E-04
	*		6	4	2.527E-03
$^{o} ightarrow i^{2}D^{e}$	0.1646	0.0422	14	10	1.557E-03
	*		8 6	6 6	1.557E-03 1.038E-04
	*		6	4	1.453E-03
$p o h^2 D^e$	0.1141	0.0524	14	10	9.500E-03
	*		8	6	9.500E-03
	*		6 6	6 4	6.333E-04 8.867E-03
$i^o \rightarrow i^2 D^e$	0.1141	0.0422	14	10	4.657E-03
	*		8	6	4.657E-03
	*		6	6 4	3.105E-04 4.347E-03
$^2F^o \rightarrow h^2D^e$	0.0836	0.0524	6 14	10	3.829E-02
1 710 12	*	0.0021	8	6	3.829E-02
	*		6	6	2.552E-03
$F^o ightarrow i^2 D^e$	0.0836	0.0422	6 14	4 10	3.573E-02 1.386E-02
$\Gamma \rightarrow i D$	**	0.0422	8	6	1.386E-02
	*		6	6	9.238E-04
$F^o o h^2 D^e$	0.0000	0.0504	6	4	1.293E-02
$F^{\circ} \rightarrow h^{\circ}D^{\circ}$	0.0639	0.0524	14 8	10 6	3.121E-01 3.121E-01
	*		6	6	2.081E-02
70 -2 50	*		6	4	2.913E-01
$i^{o} \rightarrow i^{2}D^{e}$	0.0639	0.0422	14 8	10 6	5.071E-02
	*		6	6	5.071E-02 3.381E-03
	*		6	4	4.733E-02
$i^{2}D^{e}$	0.0504	0.0422	14	10	3.893E-01
	*		8 6	6 6	3.893E-01 2.595E-02
	*		6	4	3.633E-01
$H^o o c^2 G^e$	0.1112	0.0820	22	18	7.636E-03
	*		12	10	7.636E-03
	*	:	10 10	10 8	1.697E-04 7.467E-03
$H^o \rightarrow d^2 G^e$	0.1112	0.0628	22	18	1.077E-03
	*		12	10	1.077E-03
	*	:	10	10	2.394E-05
$H^o \rightarrow e^2 G^e$	0.1112	0.0496	$\frac{10}{22}$	8 18	1.053E-03 3.286E-04
,	**		12	10	3.286E-04
	*	:	10	10	7.303E-06
$H^o \to f^2 G^e$	0.1110	0.0401	10	8	3.213E-04
1 · → J*G°	0.1112	0.0401	$\frac{22}{12}$	18 10	1.418E-04 1.418E-04
	*	•	10	10	3.152E-06
0	*	•	10	8	1.387E-04
$\rightarrow a^2 I^e$	0.1112	0.0816	22	26	2.004E+00

TABLE II. Energies and Oscillator Strengths for Allowed Transitions in Si II See page 189 for Explanation of Tables

Transition	E_{i}	E_f	g_i	g_f	f_{if}
	Ry/cm ⁻¹ 1	Ry/cm ⁻¹			
$w^2H^o \rightarrow d^2I^e$	0.0404	0.0400	00	0.0	1 FO1E 100
$w^-H^- \rightarrow a^-I^-$	0.0494	0.0400	22	26	1.591E+00
	*		$\frac{12}{12}$	14 12	1.571E+00 2.040E-02
	*		10	12	1.591E+00
$v^2H^o \rightarrow d^2I^e$	0.0400	0.0400	22	26	2.204E-02
0 11 -7 4 1	*	0.0400	12	14	2.176E-02
	*		12	12	2.826E-04
	*		10	12	2.205E-04 2.205E-02
$z^2 K^o \rightarrow c^2 I^e$	0.0625	0.0494	30	26	4.900E-03
z n ¬cı	*	0.0434	16	14	4.900E-03
	*		14	14	5.385E-05
	*		14	12	4.846E-03
$z^2 K^o \rightarrow d^2 I^e$	0.0625	0.0400	30	26	5.800E-04
2 II / u I	*	0.0400	16	14	5.800E-04
	*		14	14	6.374E-06
	*		$\hat{14}$	12	5.736E-04
$z^2 K^o \rightarrow a^2 L^e$	0.0625	0.0494	30	34	2.673E+00
	*	0.0.20.2	16	18	2.654E+00
	*		16	16	1.966E-02
	*		14	16	2.673E+00
$z^2K^o \rightarrow b^2L^e$	0.0625	0.0400	30	34	2.387E-01
	*		16	18	2.369E-01
	*		16	16	1.755E-03
	*		14	16	2.387E-01
$y^2K^o \rightarrow d^2I^e$	0.0494	0.0400	30	26	1.363E-02
v	*		16	14	1.363E-02
	*		14	14	1.498E-04
	*		14	12	1.348E-02
$y^2K^o ightarrow a^2L^e$	0.0494	0.0494	30	34	2.323E-05
-	*		16	18	2.306E-05
	*		16	16	1.708 E-07
	*		14	16	2.323E-05
$y^2K^o \rightarrow b^2L^e$	0.0494	0.0400	30	34	2.443E+00
	*		16	18	2.425E+00
	*		16	16	$1.797 ext{E-}02$
00	*		14	16	2.443E+00
$x^2K^o o b^2L^e$	0.0400	0.0400	30	34	7.167 E-05
	*		16	18	7.114E-05
	*		16	16	5.270E-07
	*		14	16	7.167E-05